

**HARMAN**

# Beam Steering & Shaping

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**AKG**

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 **Infinity**

 **JBL**

mark  
levinson

**lexicon**

 **REVEL**

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# Array myths

Arrays *must* be curved to shape the lobe...

FIR filtering to optimise the directivity of arrays is new...

Arrays can be put anywhere, the software will do the rest...

You cannot control bass...

# BASIC ARRAY PHYSICS

## What?

### WHAT IS AN ARRAY?

A loudspeaker array is a collection of sound sources (or complete enclosures) that is assembled to achieve a coverage pattern that cannot be achieved with a single loudspeaker.

The combined array is more powerful and can have a wider or narrower beam than the individual elements

### BEAMFORMING

- **Mechanical**
  - Minimum interference
  - Beam controlled by shape of array
- **Electronical**
  - Maximum interference
  - Beam controlled by (digital) signal processing of loudspeaker signals



Line array



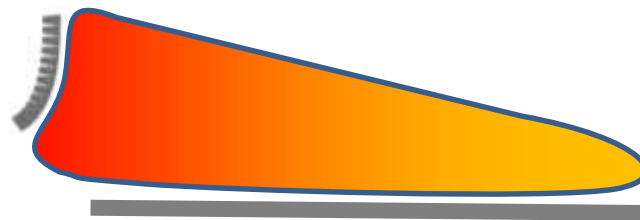
Beam steered/shaped column

# ARRAY PHYSICS

## Beamforming Concepts

- **Mechanical beamforming**

- Line arrays: Radiation pattern dictated by shape of array.
- Minimum interference. HF horns are designed to have minimum mutual interference at higher frequencies.
- Low driver density.
- No multi-channel signal processing.



- **Electronical beamforming**

- Radiation pattern determined by (digital) filtering of output channels (i.e., loudspeaker signals)
- High driver density.
- Maximum interference: Deliberate, controlled interference for obtaining desired radiation pattern.



# ARRAY PHYSICS

## Sound Waves

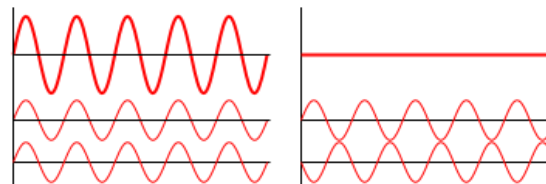
### KEYWORDS:

- Sound is a wave phenomenon
  - Frequency  $f$
  - Wave length  $\lambda$
  - Speed of sound  $c$  (=340 m/s)

$$\lambda = \frac{c}{f}$$

$f$ [Hz]	20	50	100	200	500	1000	2000	5000	10000	20000
$\lambda$ [m]	17.0	6.8	3.4	1.7	0.68	0.34	0.17	0.068	0.034	0.017

- Waves interfere



Constructive

Destructive

# ARRAY PHYSICS

## Interference

- A small loudspeaker (monopole) radiates sound in all directions (omni-directional sound wave).
- By combining several loudspeakers in an array, the radiation pattern becomes directional.
- In the target direction the sound waves sum, in other directions they (partially) cancel.

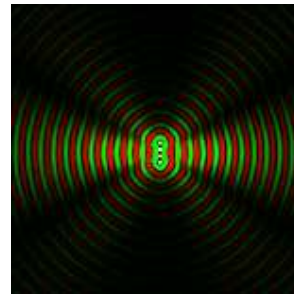
1 monopole



2 monopoles spaced at  $\lambda/2$



4 monopoles spaced at  $\lambda/2$



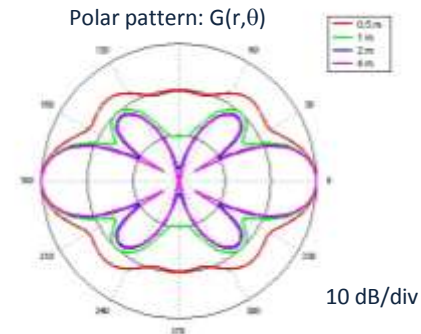
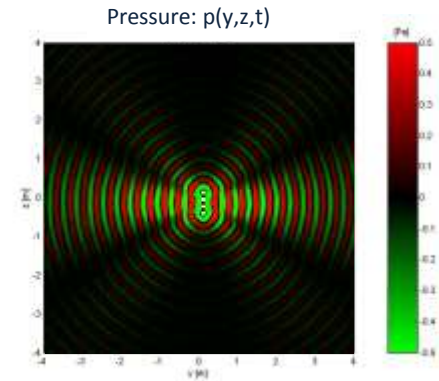
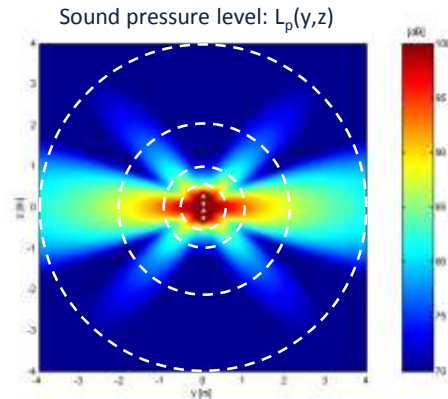
# ARRAY PHYSICS

## Interference

### 4 monopoles ( $f=1\text{kHz}$ , spacing= $\lambda/2$ )

#### Representation:

- Space-time ( $yz-t$ )
- Space-frequency ( $yz-f$ )
- Angle-frequency ( $r\theta-f$ )

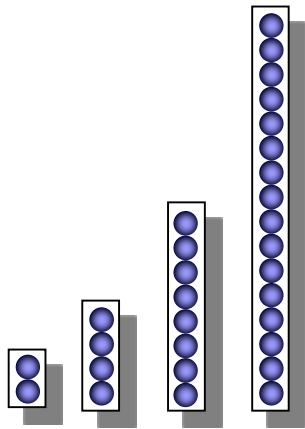




# ARRAY PHYSICS

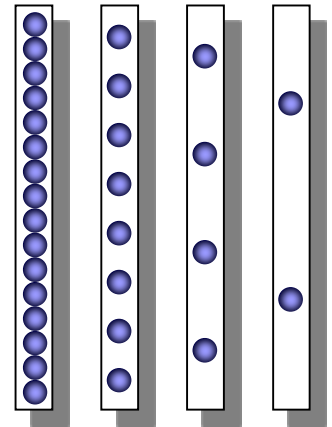
## Length and Spacing

### BEHAVIOUR OF A PARALLEL-DRIVEN POINT SOURCE ARRAY

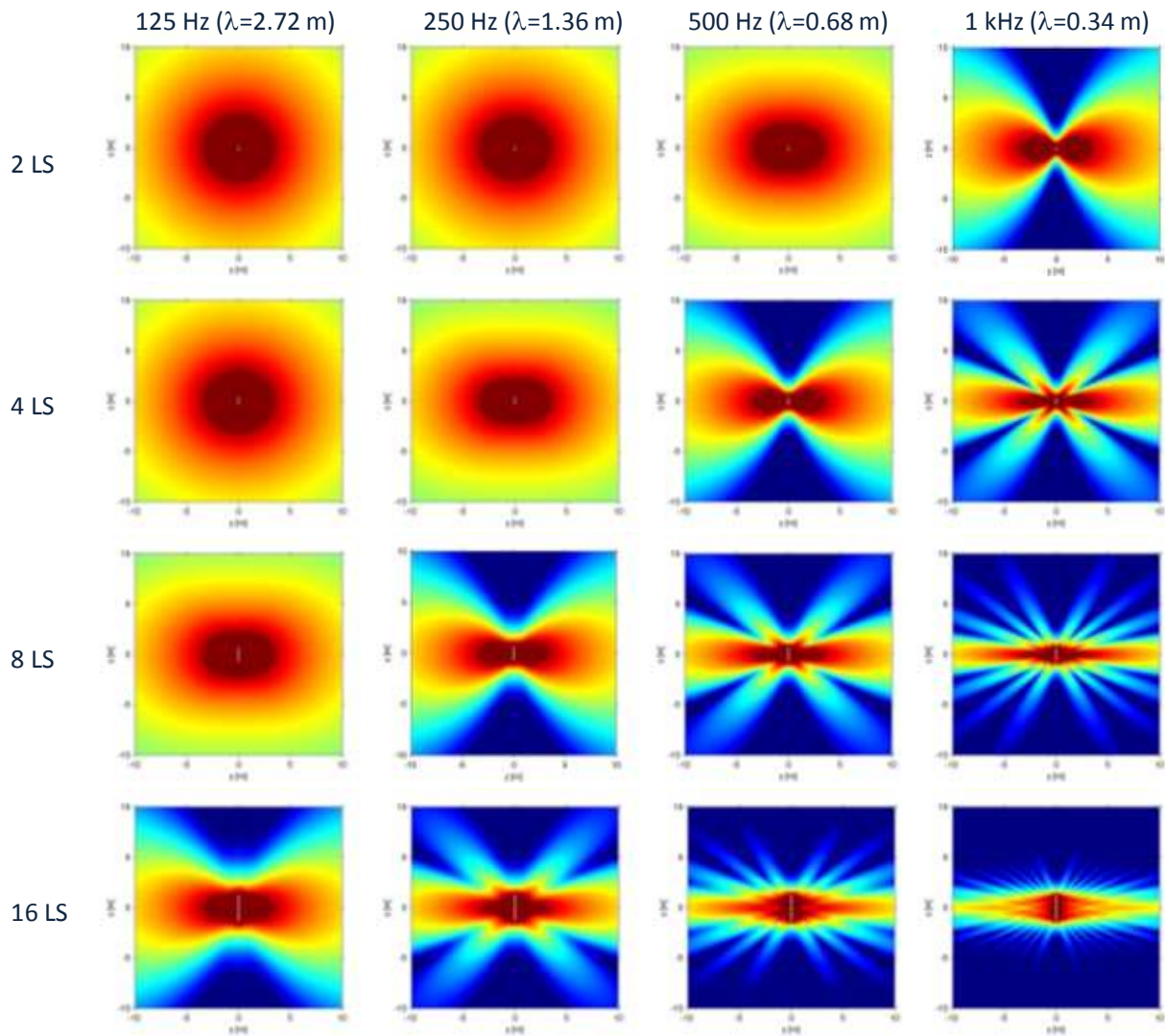
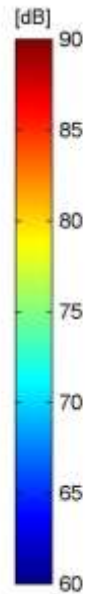


Fixed driver spacing,  
variable array length

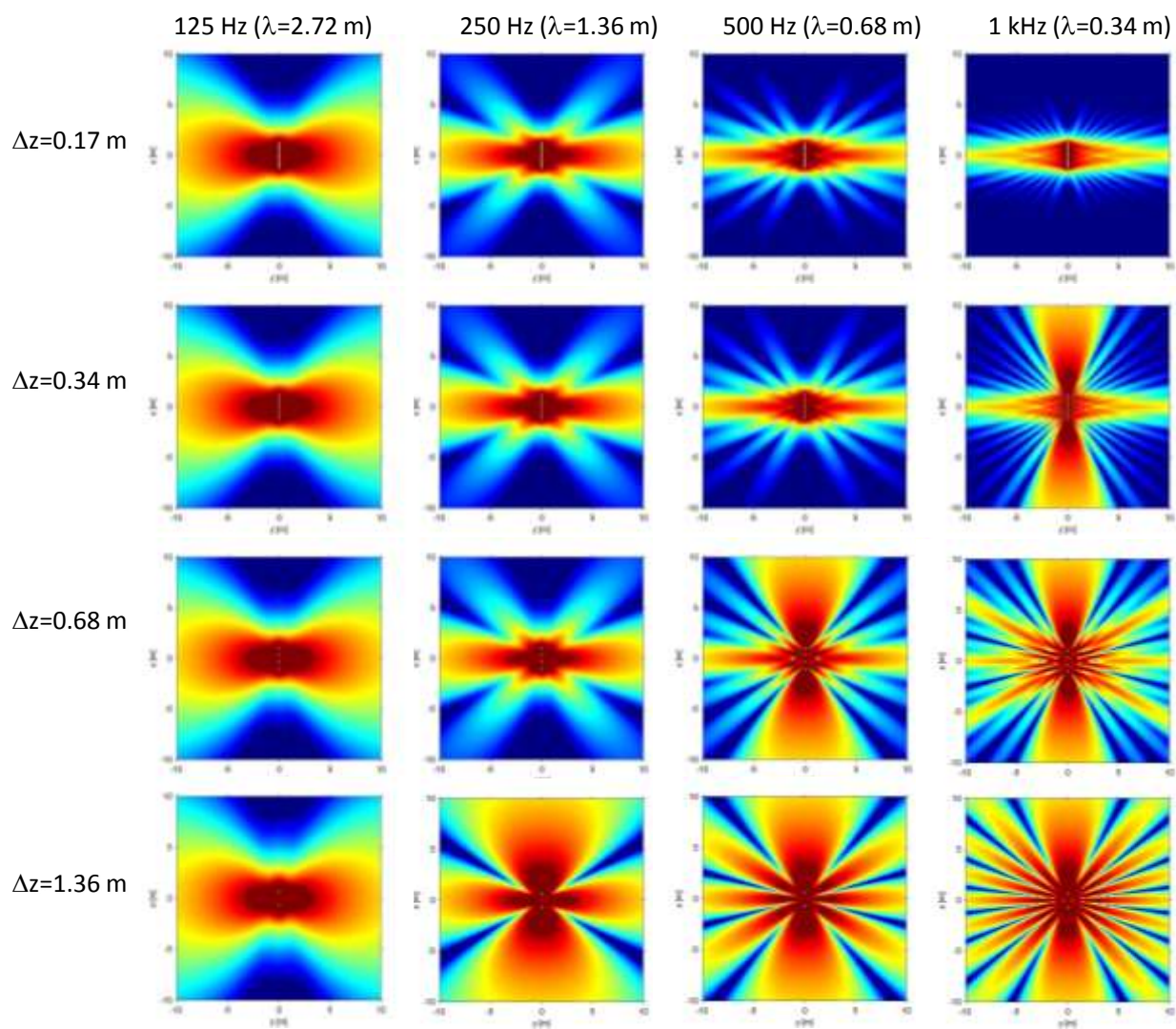
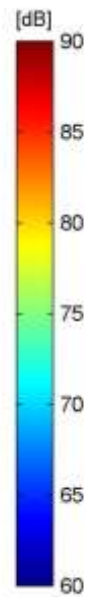
Fixed array length,  
variable driver spacing



$\Delta z = 0.17$  m



$L=2.72$  m



# ARRAY PHYSICS

## Basic Laws

- Effect of array size and wave length:

$$\text{Beam width} \sim \frac{\lambda}{L}$$

- Spatial sampling (i.e. driver spacing):

$$\Delta z \leq \frac{\lambda}{2}$$

(Nyquist criterion)

- ❖ Note: For directional sources like waveguides this anti-aliasing criterion can be relaxed

# DIRECTIVITY CONTROL

## Beamforming technology

### AS SHOWN, THERE IS A NEED FOR DIRECTIVITY CONTROL

#### Objectives:

- Consistent radiation pattern over frequency
- Uniform coverage and frequency response
- Minimize “spill” (e.g., avoid reflective surfaces or reduce outdoor noise pollution)

#### Methods:

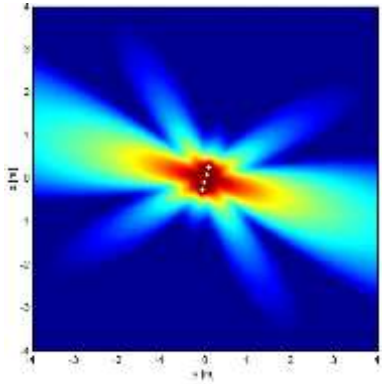
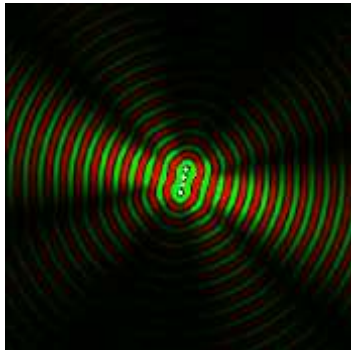
- Mechanical line array optimisation
  - Signal processing
    - “constant- $\lambda$ ” design, i.e.  $L_{\text{eff}} = C \cdot \lambda$
    - Beam steering
    - Beam shaping
- Minimum interference
- Maximum interference

# DIRECTIVITY CONTROL

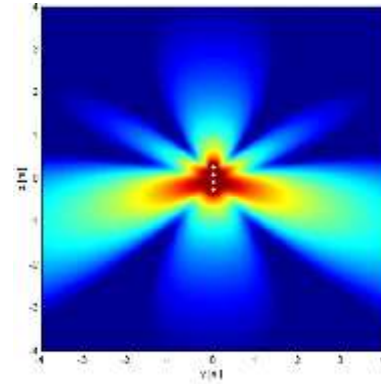
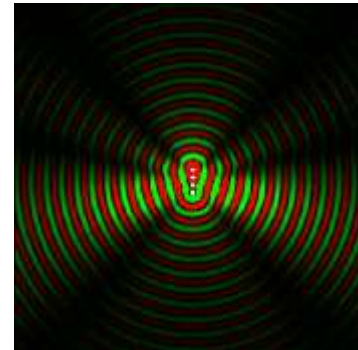
## Beam Steering

Mechanical Aiming  
versus  
Electronic Steering

Mechanical  
aiming



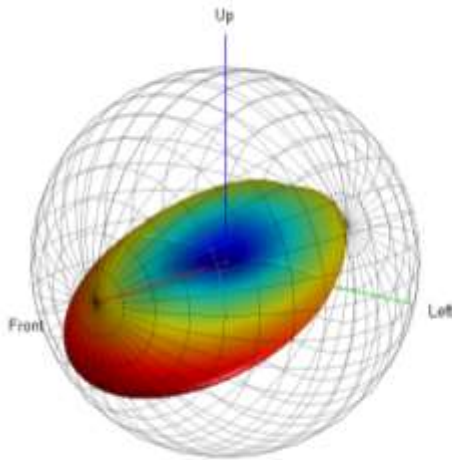
Electronic  
steering



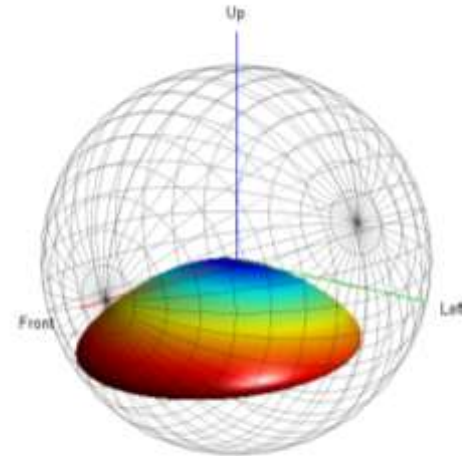
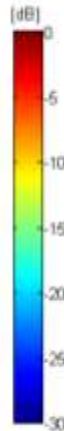
# DIRECTIVITY CONTROL

## Beam Steering

### Mechanical aiming versus electronic steering



Mechanical aiming

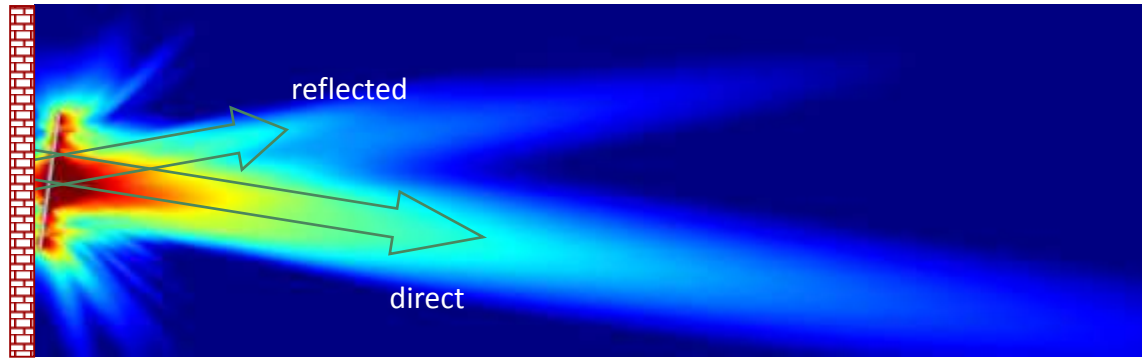


Electronic steering

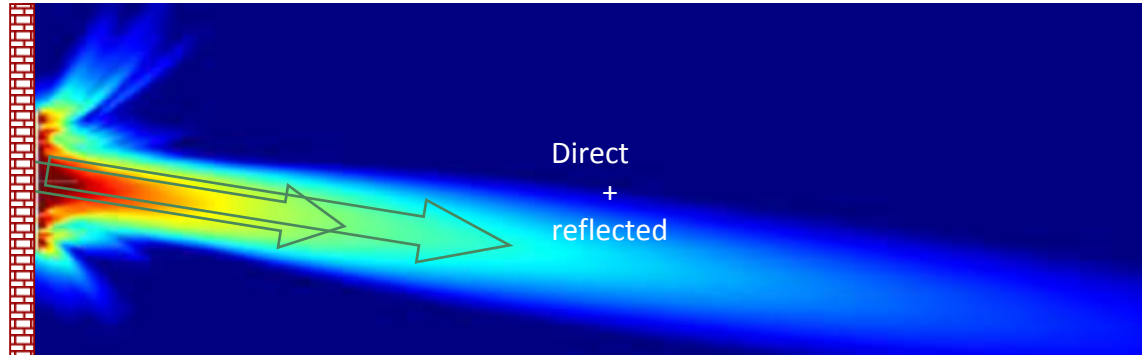
# DIRECTIVITY CONTROL

## Beam Steering

Mechanical aiming



Electronic steering





# DIRECTIVITY CONTROL

## Some History

Early attempts to control the opening angle (“constant- $\lambda$ ”):

- Electrical Low-pass filter circuit
- Mid/wide band loudspeaker arrangement
- Barber pole
- Acoustic low-pass filtering

# DIRECTIVITY CONTROL

## Some History

Electro-Voice LR-4S (1950s)

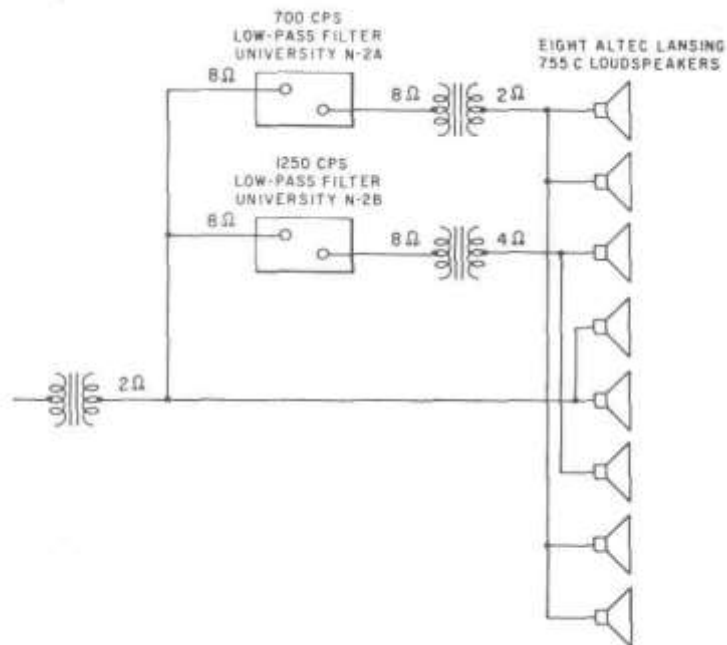


FIG. 1. Line-source loudspeaker with electrical filtering at Franklin Hall, Franklin Institute, Philadelphia, Pa.

# DIRECTIVITY CONTROL

## Some History

UL (1950s)

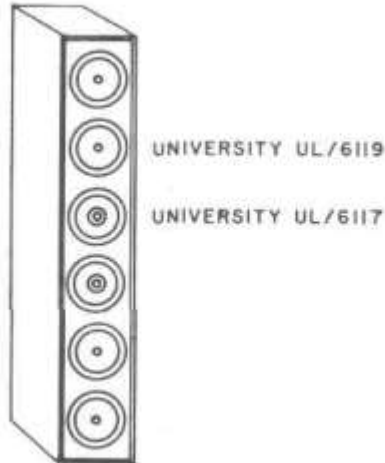


FIG. 2. Line-source loudspeaker with omission of high frequency "whizzer" in outer loudspeakers; University loudspeaker UCS-6.

# DIRECTIVITY CONTROL

## Some History

“Barber pole” (Philips 1958)



FIG. 3. “Barber pole” line source: Palais Chailot, Philips system.

# DIRECTIVITY CONTROL

## Some History

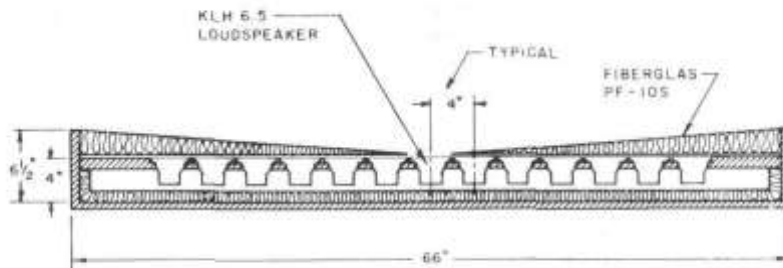


FIG. 4. Section through line-source loudspeaker (enclosure is made of  $\frac{3}{4}$  in plywood).

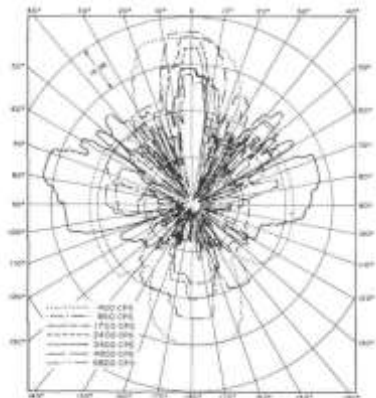


FIG. 6. Polar plot line source containing 13 4-in loudspeakers, on glass fiber.

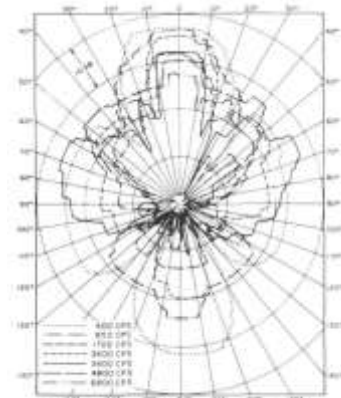


FIG. 7. Polar plot line source containing 13 4-in loudspeakers with glass fiber angles.

# DIRECTIVITY CONTROL

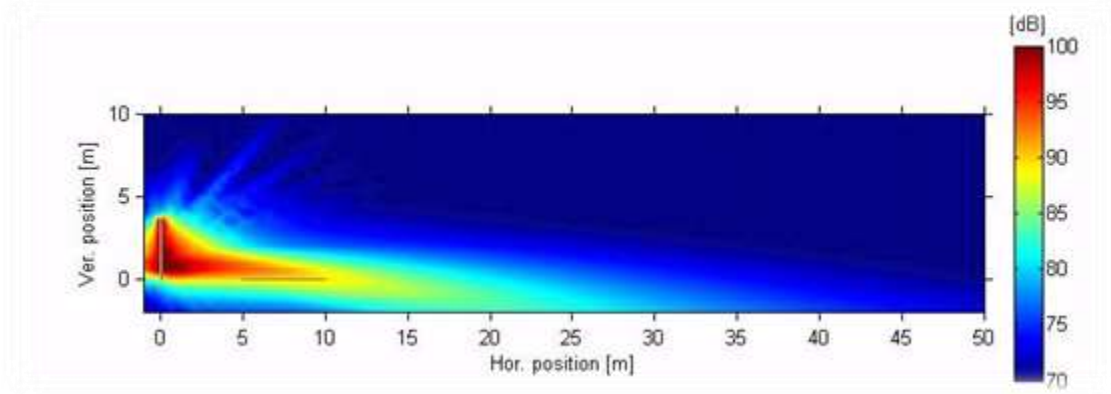
## Advanced techniques

### 1. DDC – BEAM STEERING

(Developed and introduced in the early 90-ies by Duran Audio)

### 2. DDS – BEAM SHAPING

(Developed and introduced in 1999)

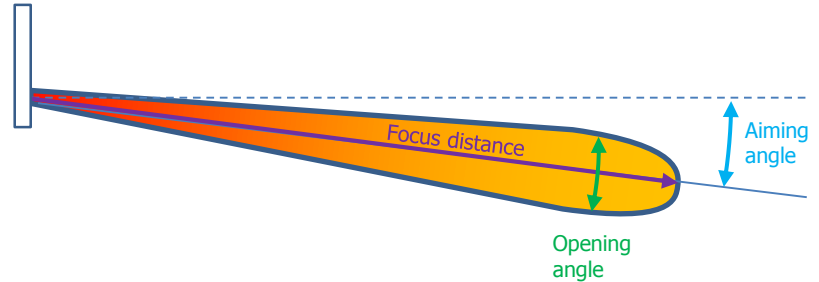


# DDC BEAM STEERING

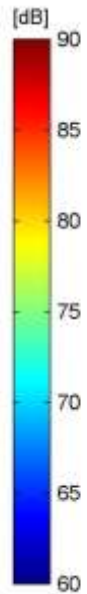
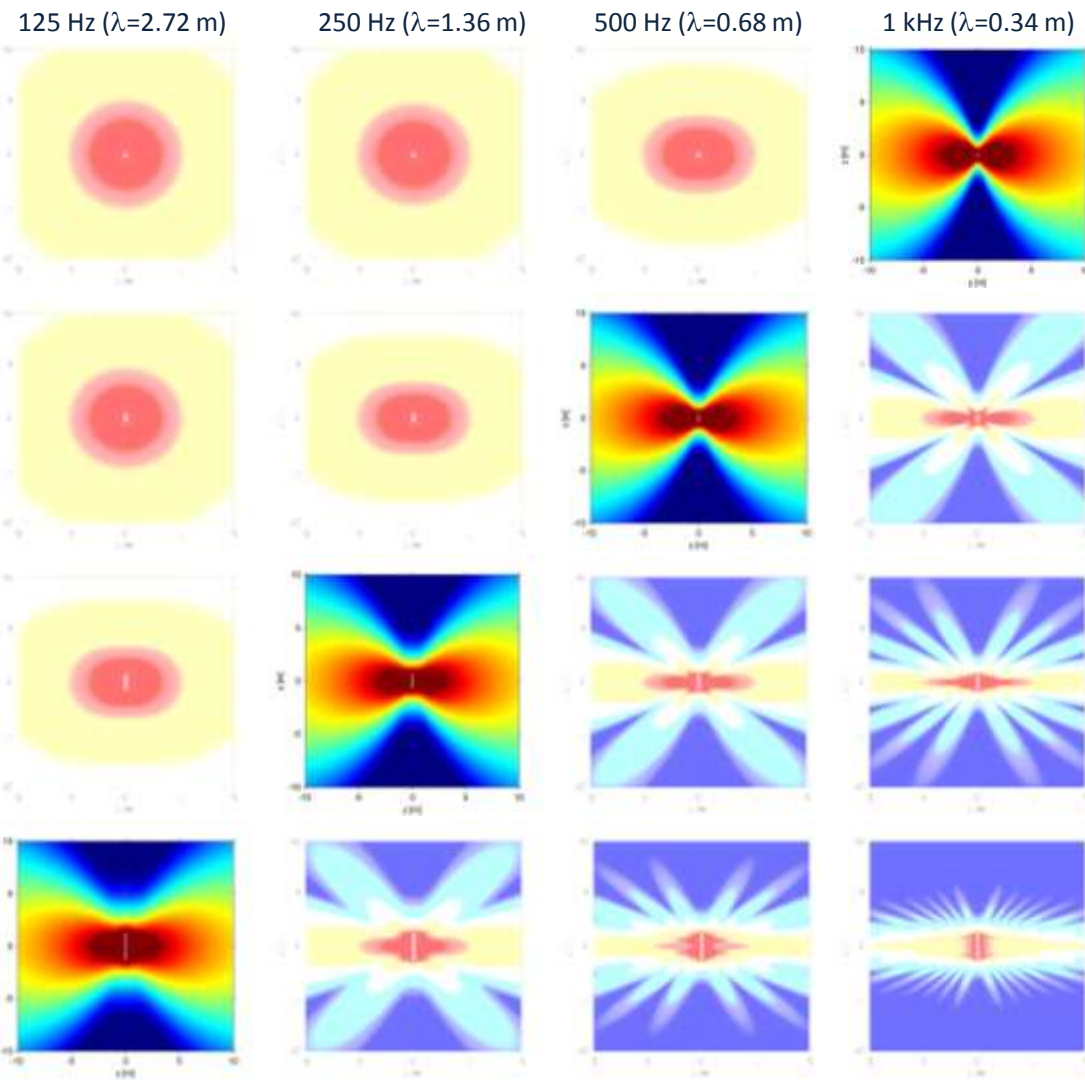


## Digital Directivity Control (DDC)

- "Beam Steering"
- Parametric beam control
- Applied in:
  - Intellivox-DC range



$L=1\lambda$   
 $\Delta z = 0.17 \text{ m}$





$L = 1\lambda$   
 $\Delta z = \lambda/2$

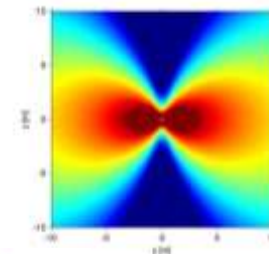
125 Hz ( $\lambda = 2.72$  m)

250 Hz ( $\lambda = 1.36$  m)

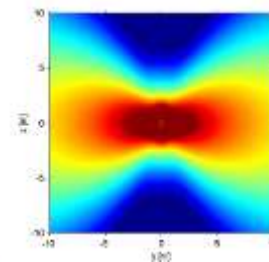
500 Hz ( $\lambda = 0.68$  m)

1 kHz ( $\lambda = 0.34$  m)

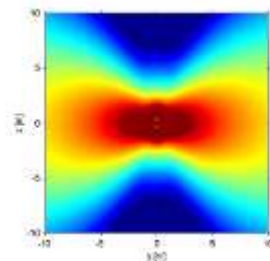
2 LS



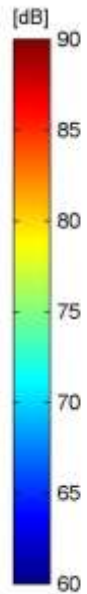
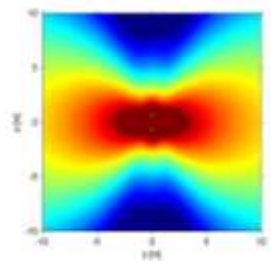
4 LS



8 LS



16 LS



# DDC - BEAM STEERING

## Transducer spacing

Frequency independent:

+

$$L_{eff}(\lambda) = const \cdot \lambda$$

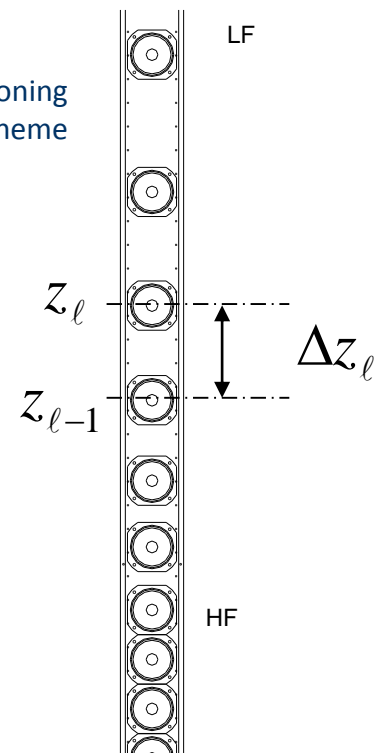
Logarithmic positioning:

⇓

$$\Delta z_\ell \leq \frac{\lambda_{min}}{2}$$

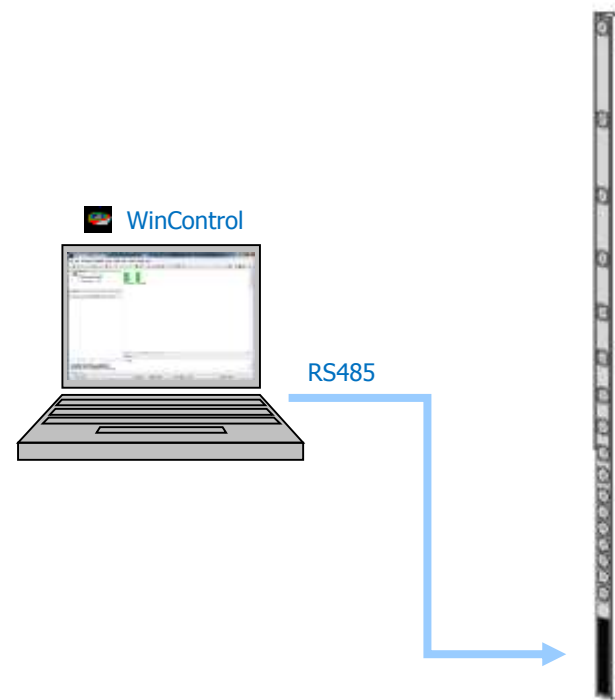
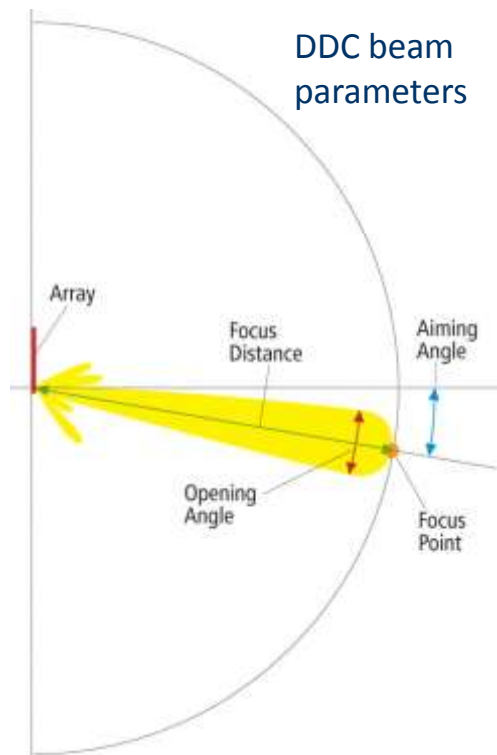
Reduction of the number of loudspeakers and signal processing for a given array length

Patented positioning scheme



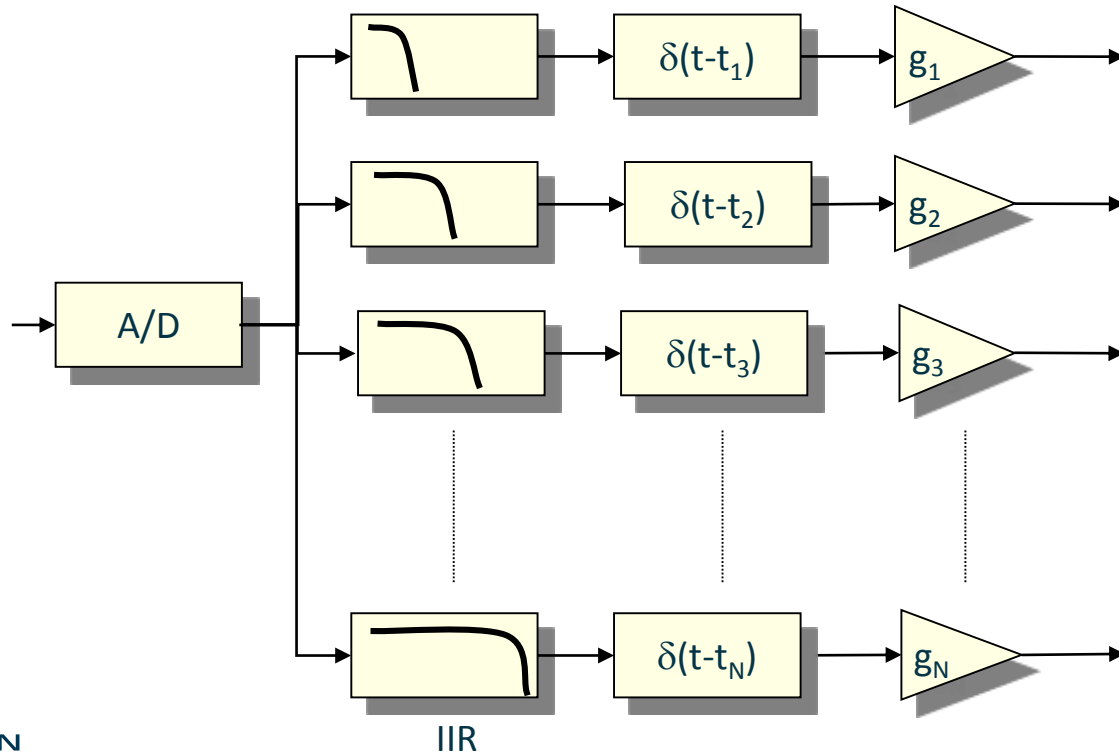
# DDC - BEAM STEERING

## Beam parameters



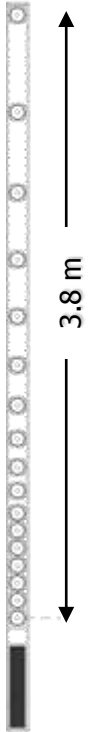
# DDC - BEAM STEERING

## Block diagram



# DDC - BEAM STEERING

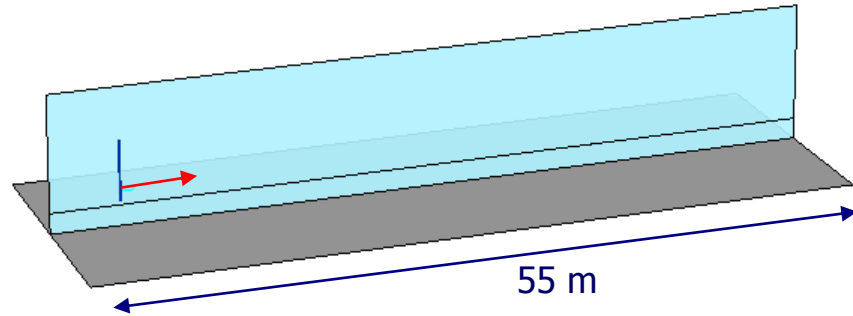
## Example



$$z_c = 2.5 \text{ m}$$

$$z_{ij} = 1.7 \text{ m}$$

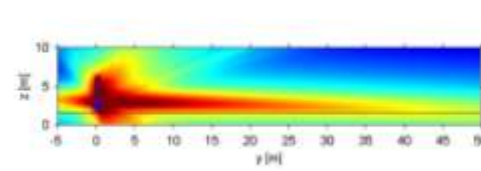
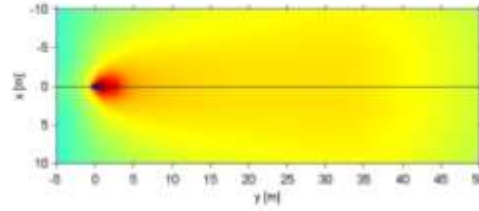
Geometry



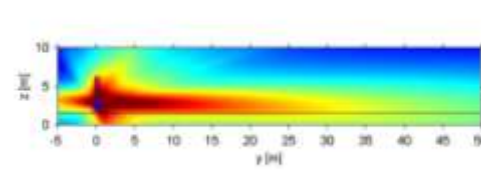
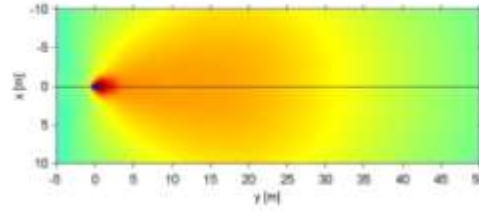
Plan view

Side view

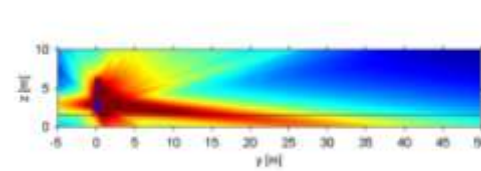
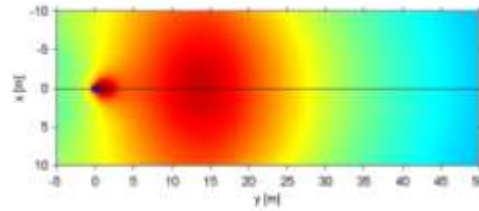
Opening Angle:  $6^\circ$   
 Elevation:  $-1^\circ$   
 Focus distance: 50 m



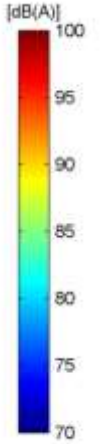
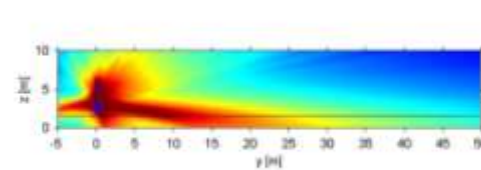
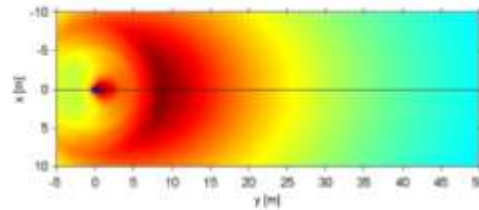
Opening Angle:  $14^\circ$   
 Elevation:  $-1^\circ$   
 Focus distance: 50 m



Opening Angle:  $6^\circ$   
 Elevation:  $-5^\circ$   
 Focus distance: 50 m

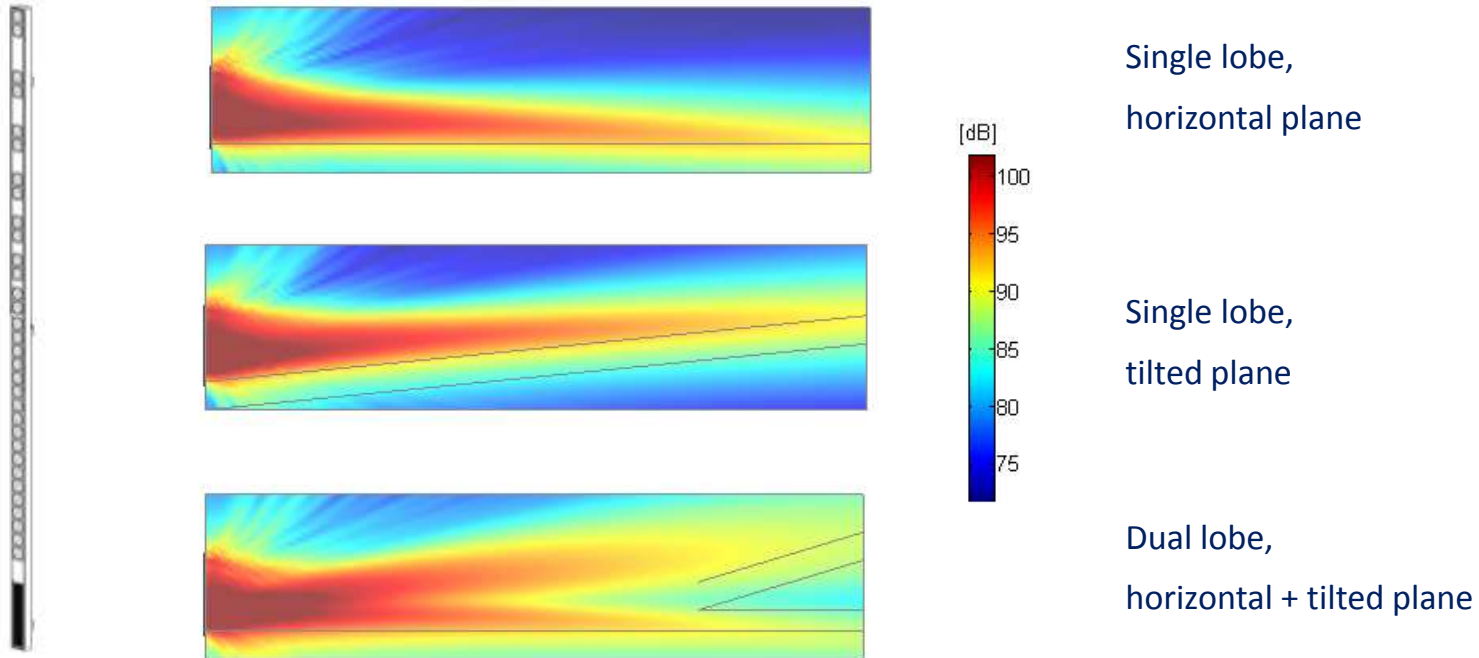


Opening Angle:  $6^\circ$   
 Elevation:  $-1^\circ$   
 Focus distance: 10 m



# DDC - BEAM STEERING

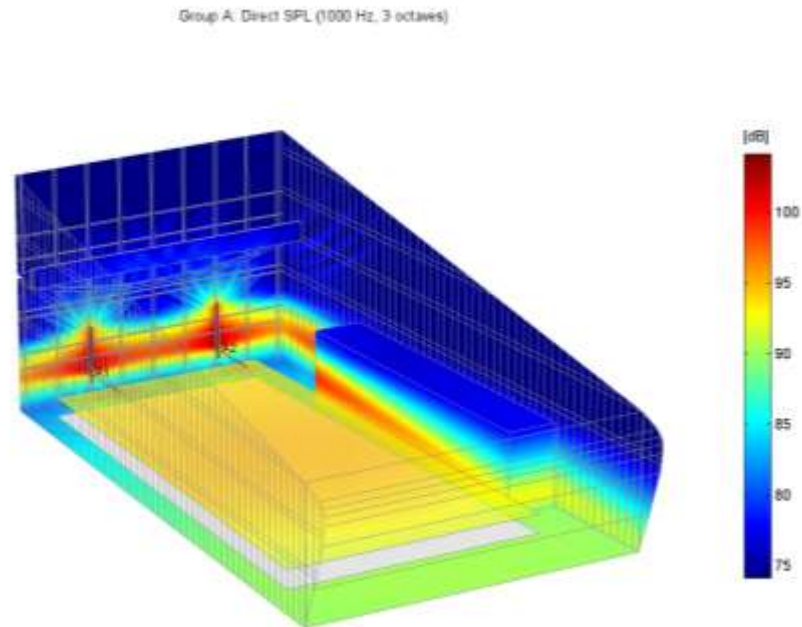
## Typical use



# DDC - BEAM STEERING

## Features

- Simple and intuitive parametric control
  - Opening angle
  - Aiming angle
  - Focus distance
- Constant SPL over distance (up to 70m)
- Large direct-to-reverberant ratio
- High speech intelligibility
- Most suitable for flat audience areas
- Mounting height restrictions:
  - Offset between acoustic center and audience plane  
0.3-0.6 m (~ 1-2 ft.)

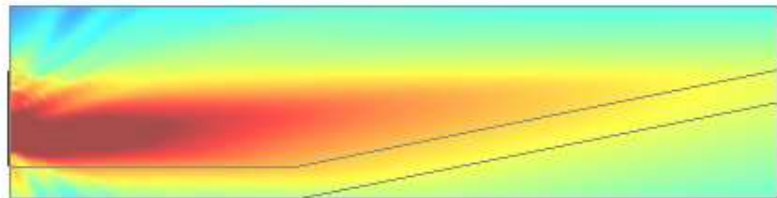
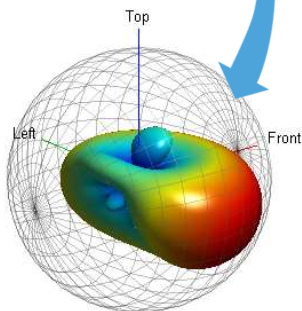




# BEYOND BEAM STEERING...

## What if:

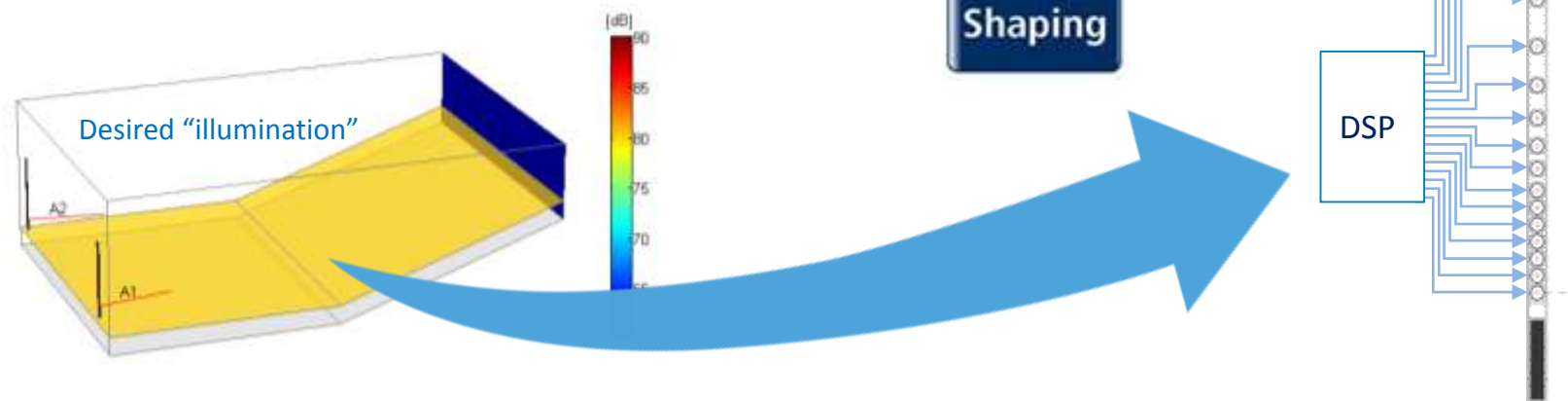
- we could not only steer but also **shape** the beam?
- we could **extend** the frequency response?
- we could control **bass**?



# DDS - BEAM SHAPING

## The Inverse Approach

- Digital Directivity Synthesis (DDS)
- Invert the desired “illumination” of the room to the array.
- Boundary conditions:
  - Minimum sound power
  - minimum “spill”
  - Robustness & Stability



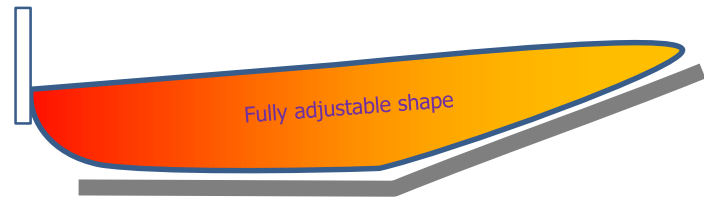
# DDS

## BEAM SHAPING



### Digital Directivity Synthesis (DDS)

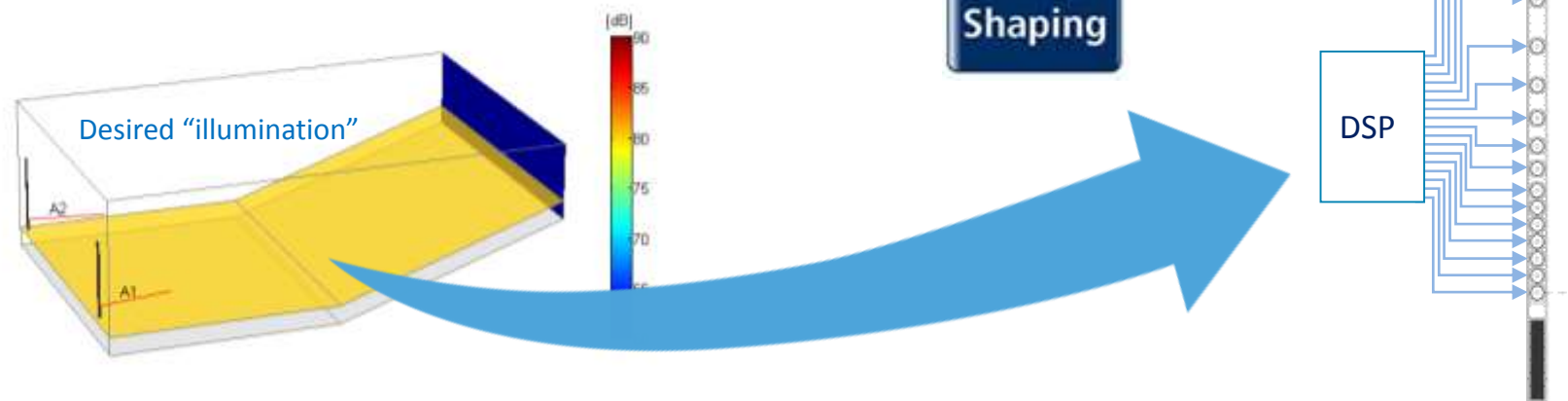
- “Beam Shaping”
- Beam can be adapted to geometry of the room
- Applied in:
  - Intellivox-DS(X) range



# DDS - BEAM SHAPING

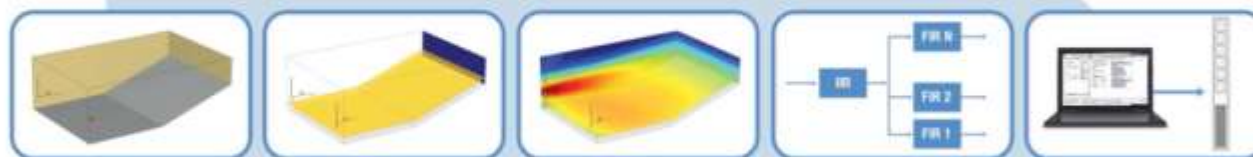
## The Inverse Approach

- Digital Directivity Synthesis (DDS)
- Invert the desired “illumination” of the room to the array.
- Boundary conditions:
  - Minimum sound power
  - minimum “spill”
  - Robustness & Stability



# DDS - BEAM SHAPING

## DDS Workflow



### 3D Geometry

- SketchUp
- DDA 2D builder

### Design Input

- Room acoustic properties
- Loudspeakers
- Desired coverage

### Simulation

- 3D rendering of results
- Verify/modify design

### Full calculation

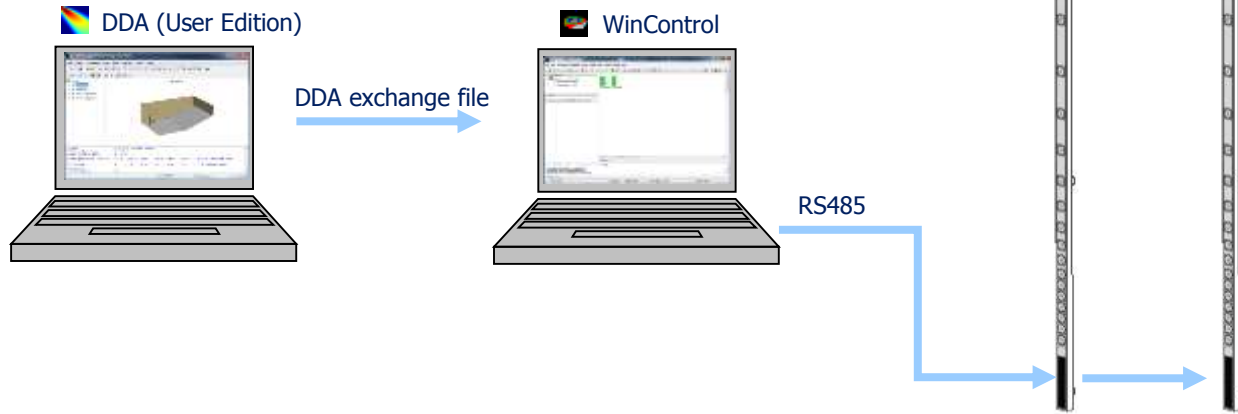
- Optimum output filters
- Low-latency FIR design

### Connect to network

- Upload filters to unit
- EQ
- Surveillance

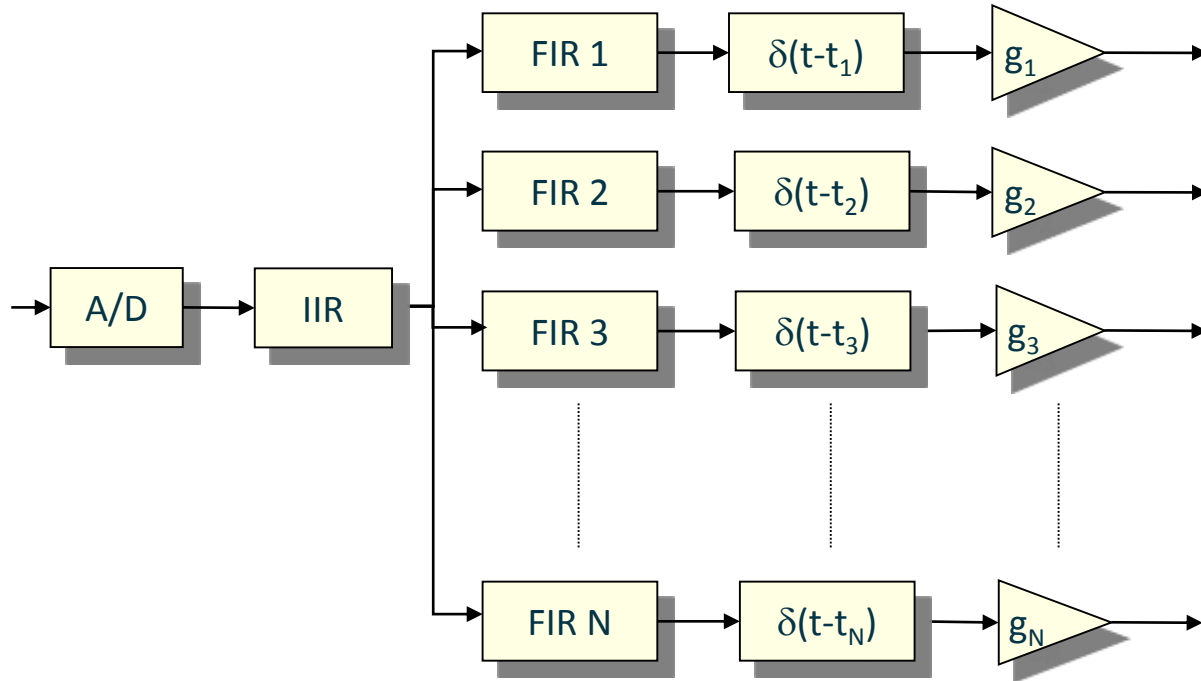
# DDS - BEAM SHAPING

## Upload Process



# DDS BEAMFORMING

## Block Diagram



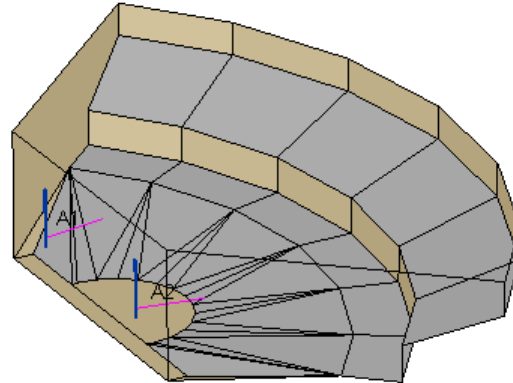
# DDS - BEAM SHAPING

## Intellivox Application Example

### SWEDISH PARLIAMENT

- Fan-shaped hall
- Reflective curved back wall
- 2x Intellivox-4c-XL (predecessor of Intellivox-DS430)

Geometry





# DDS INTELLIVOX

## Intellivox Application Example

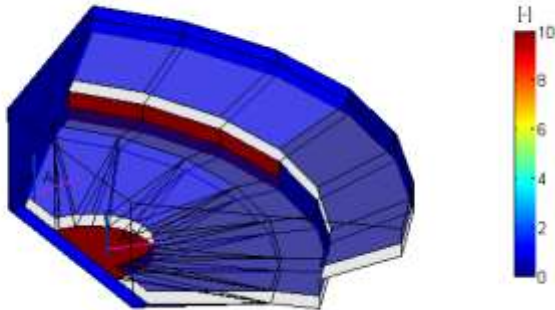
- Swedish Parliament
  - Fan-shaped hall
  - Reflective curved back wall



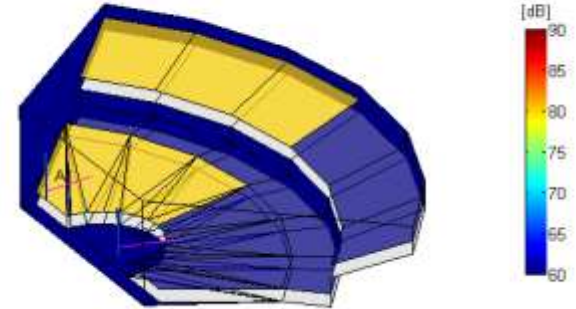
# DDS - BEAM SHAPING

## Intellivox Application Example

Weights (priority factors)



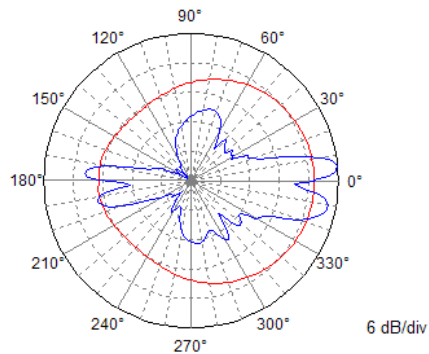
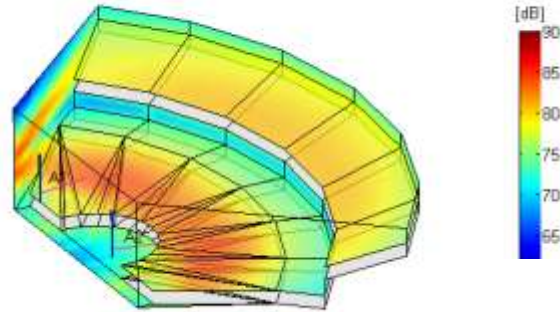
Desired direct SPL distribution



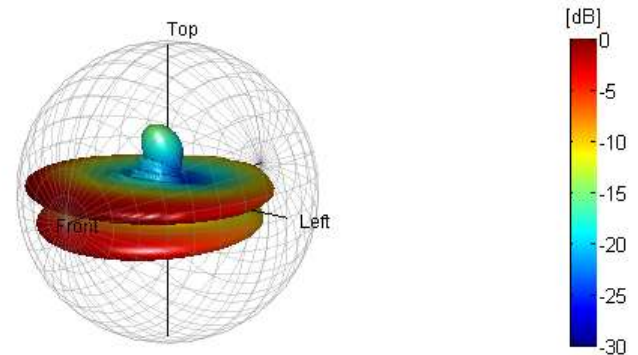
# DDS - BEAM SHAPING

## Intellivox Application Example

Realized direct SPL distribution



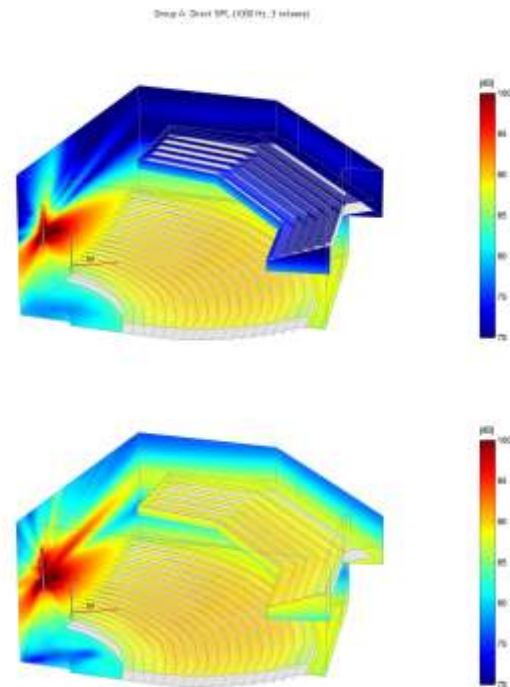
Far field polar pattern



# DDS - BEAM SHAPING

## Features

- Flexible array set-up
- Tailor-made directivity pattern
  - Requires (basic) 3D geometric model of space → SketchUp<sup>®</sup> + Plugin
- Constant spectral balance for all listening positions
- Optimum direct-to-reverberant energy ratio
- Both far field and near field control
- Directivity pattern can be changed by software, i.e., without re-angling the boxes



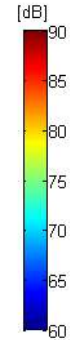
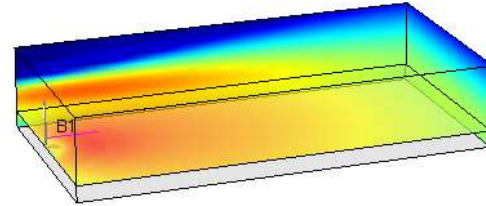
# DDS - BEAM SHAPING

## Mounting height vs. Coverage

Intellivox-DS430

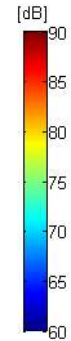
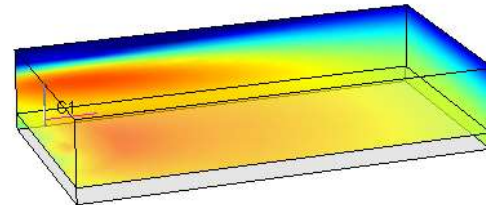
$H=2.5$  m

$\Delta z = 0.8$  m



$H=4.5$  m

$\Delta z = 2.8$  m



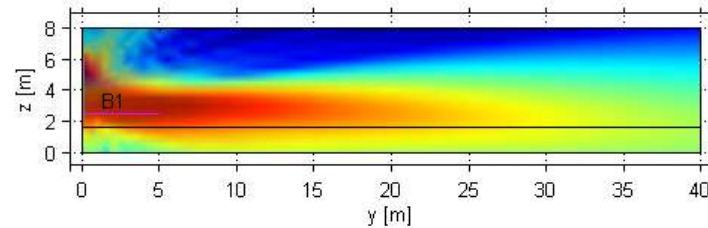
# DDS - BEAM SHAPING

## Mounting height vs. Dispersion

Intellivox-DS430

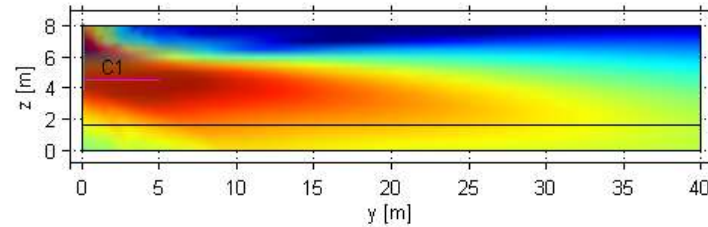
$H=2.5$  m

$\Delta z = 0.8$  m



$H=4.5$  m

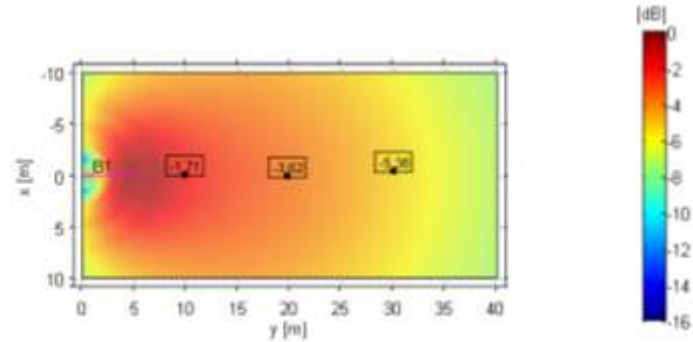
$\Delta z = 2.8$  m



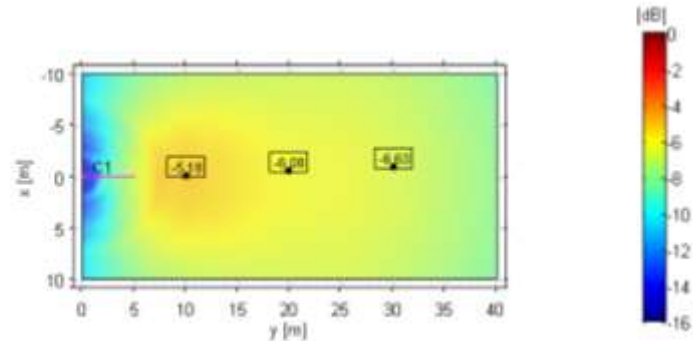
# DDS - BEAM SHAPING

## Mounting height vs. D/R ratio

$\langle D/R \rangle = -4.6$  dB



$\langle D/R \rangle = -7.0$  dB



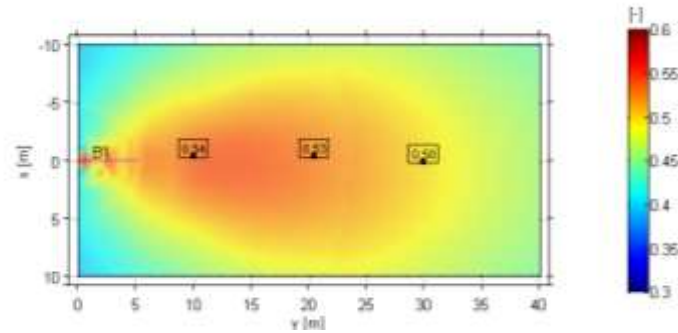
$V=6,400$  m<sup>3</sup>

RT=3 s

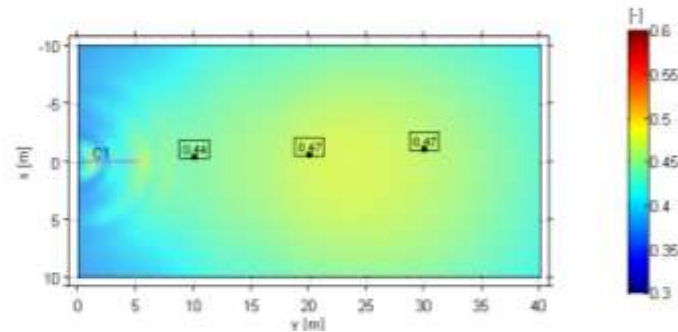
# DDS - BEAM SHAPING

## Mounting height vs. Intelligibility

$\langle \text{STI} \rangle = 0.50$



$\langle \text{STI} \rangle = 0.45$



$V = 6,400 \text{ m}^3$

$RT = 3 \text{ s}$



# DDS - BEAM SHAPING

## Mounting height

### Conclusion:

- Larger mounting height
  - Larger steering angle & wider dispersion
  - Lower D/R ratio
  - Poorer speech intelligibility and musical clarity

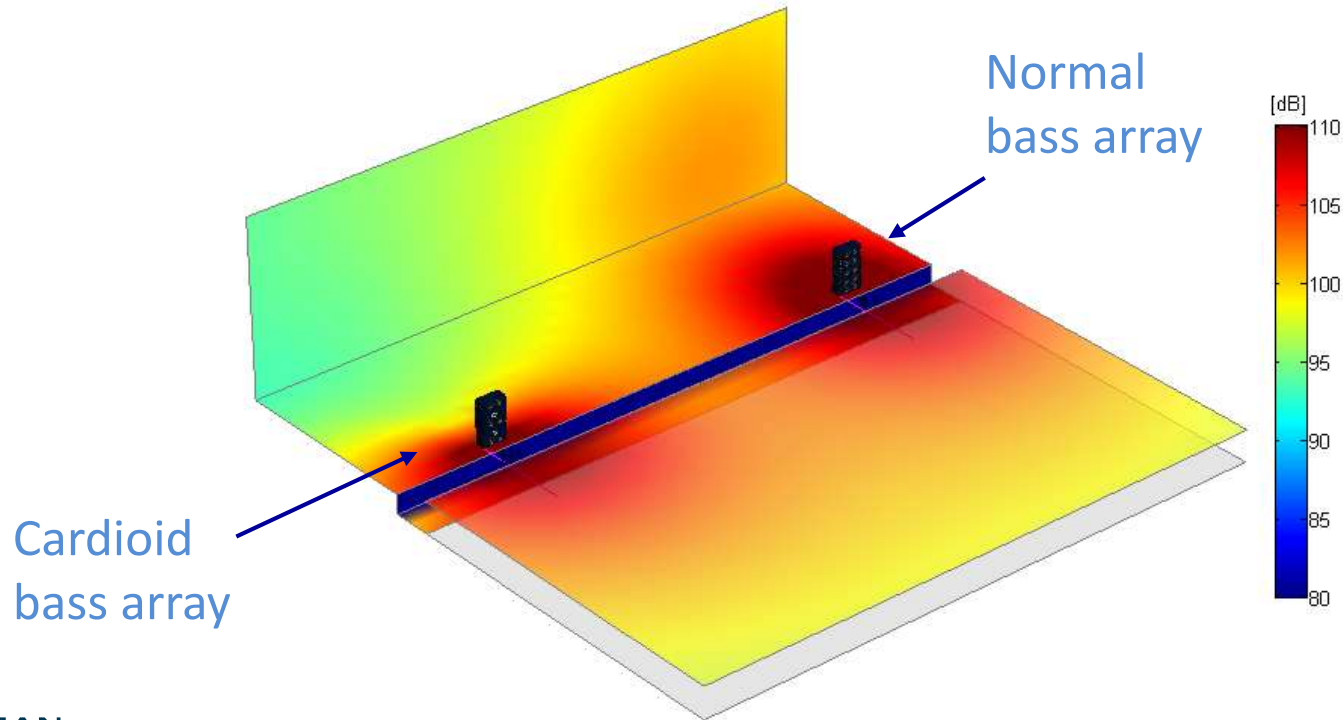
Extremely large steering angles don't make sense!

# CONTROLLING BASS

- 1. WHAT ARE BEAM-SHAPED DIFFERENTIAL SUBWOOFER ARRAYS?**
- 2. ACOUSTIC MODELLING BY PSM-BEM**
- 3. VALIDATION OF PSM-BEM BY MEASUREMENTS**
- 4. SUMMARY AND CONCLUSIONS**



# Normal versus cardioid bass arrays



# SUBWOOFER ARRAYS

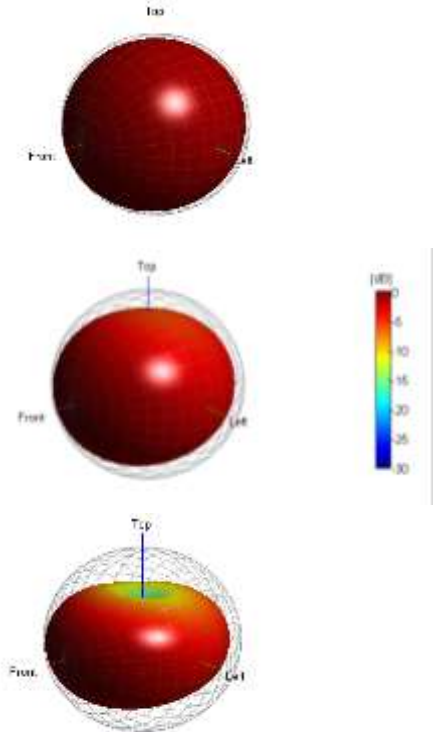
## “Summing”

Directivity:

$$Q \propto \frac{L}{\lambda} \quad DI = 10 \log(Q)$$

Gain and robustness:

$$G_{array} = 10 \log \left[ \frac{P_{array}^2(f)}{\sum_{l=1}^L P_l^2(f)} \right]$$

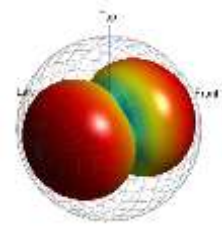
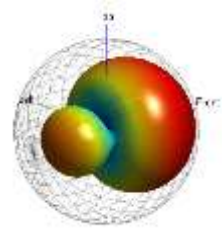
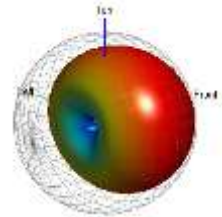


# SUBWOOFER ARRAYS

## “Differential”

- + “Superdirectional”, i.e., high Q for small  $L/\lambda$
- Less robust than delay-and-sum arrays

80 Hz



1x B-215DIFF



Front

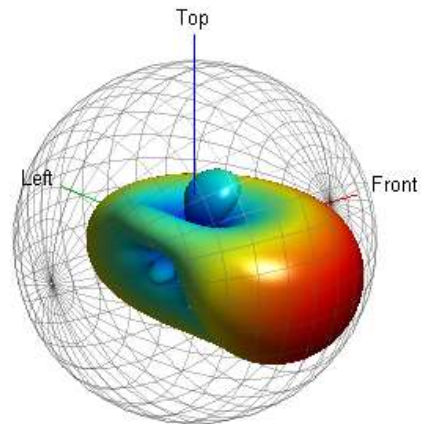
Back

3x B-07



# BEAM-SHAPED DIFFERENTIAL SUBWOOFER ARRAYS

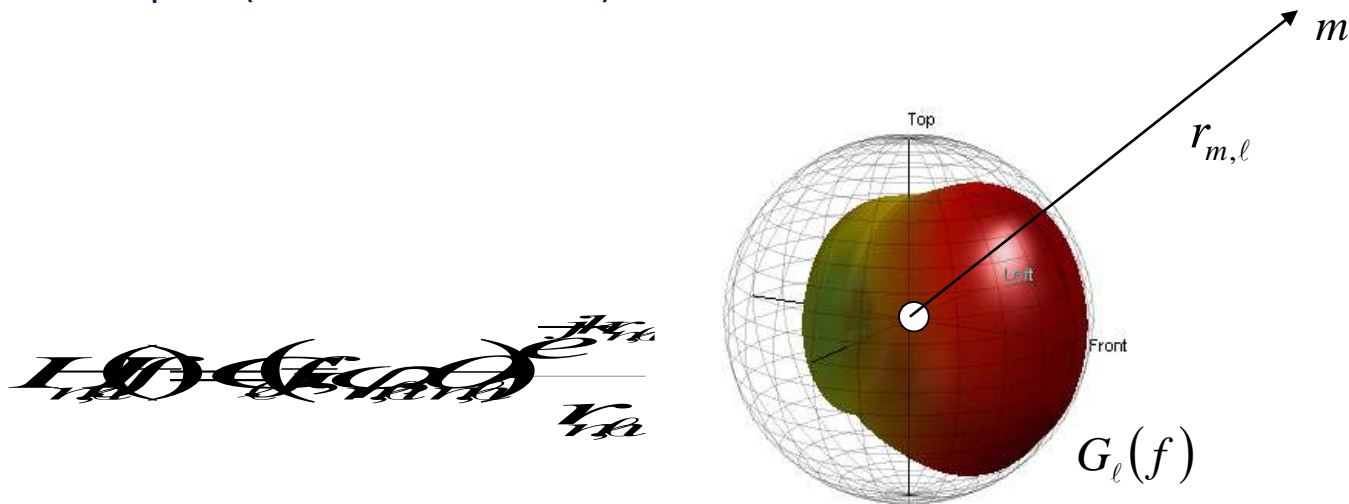
- Combination of delay-and-sum and differential array
- DDS-optimised
  - Requires an accurate model of each box



# ACOUSTIC MODELLING OF SUB ARRAYS

## Point Source Model (PSM)

- Each loudspeaker in the array is represented by a point source with a certain directivity
- Radiation into free space (free field conditions)



# POINT SOURCE MODEL (PSM)

## Benefits:

- Computationally efficient
- Only one directivity function for each loudspeaker type

## Shortcomings:

- No LF 'coupling' between stacked subwoofers
  - In reality, sensitivity of each box depends on stack size
- No modelling of LF diffraction around array
  - In reality, directivity and F/B ratio of each box depends on stack size
- No accurate ground plane modelling (i.e., half-space) possible with simple mirror image source model

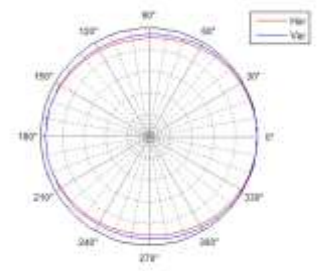


# COUPLING EFFECTS

## ARRAY SIZE AND LOUDSPEAKER POSITION



Free field ↓



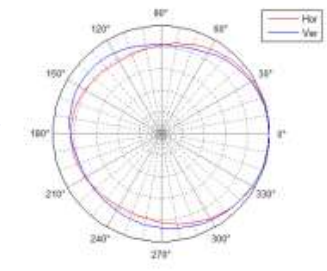
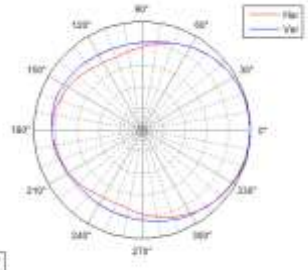
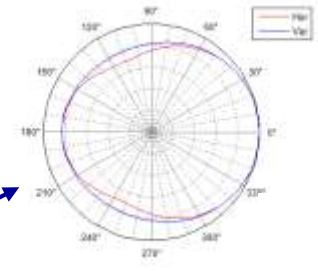
Magnitude (6 dB/div)



5U3

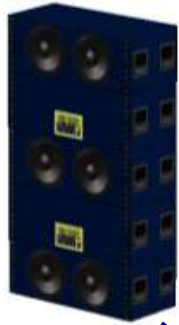
5U2

5U1



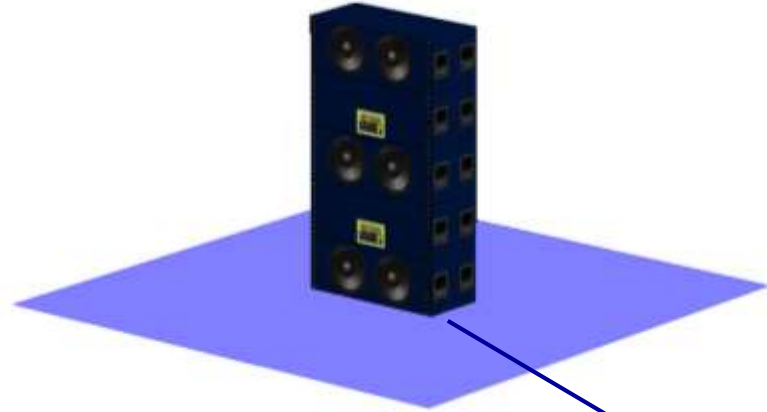
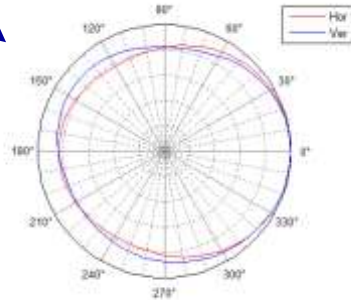
# COUPLING EFFECTS

Boundary plane



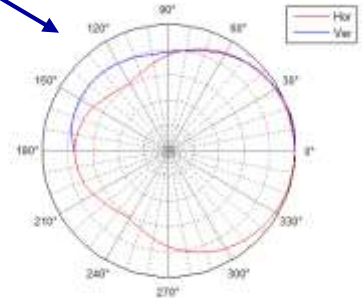
Full-space

5U1  
FS



Half-space

5U1  
HS



Magnitude (6 dB/div)

# HYBRID PSM-BEM MODEL

## Idea:

- Each loudspeaker in the array is modelled as a directional point source
- BEM is applied to calculate directivity functions of loudspeaker facing the actual Acoustic Boundary Conditions (ABC), including half space conditions

## Benefits:

- One-time only calculation of directivity library for various ABC
- Library can be easily extended
- Computationally efficient simulation

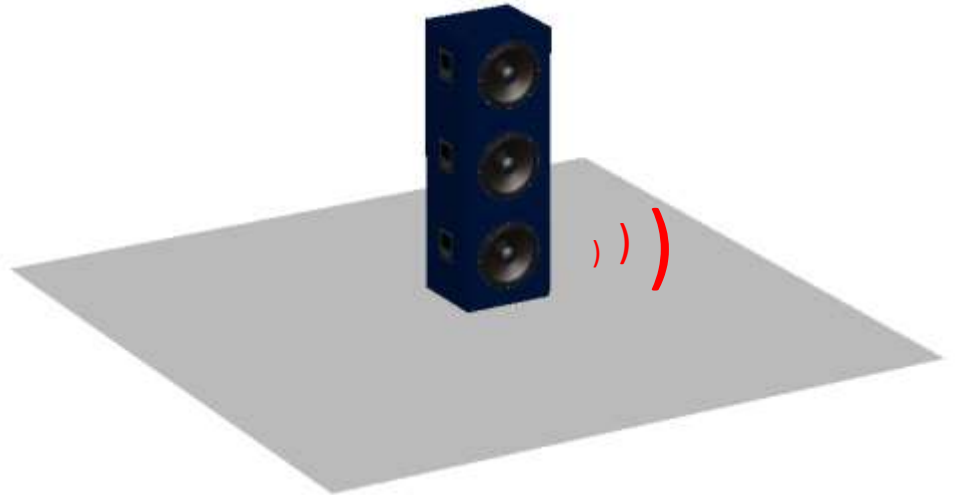
# BEM CALCULATIONS

## Procedure:

- Measure normal component of particle velocity in front of cone and ports of subwoofer
- Make finite boundary element model of subwoofer array
- Calculate pressure distribution on boundaries using either full-space or half-space version of Helmholtz Integral Equation (HIE)
- From the measured velocity and the calculated pressure distribution, calculate directivity balloons for active subwoofer

# BEM CALCULATION EXAMPLE

Set-up



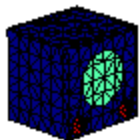
Free-Field

3U1 full-space

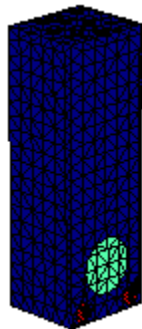
3U1 half-space

# BEM CALCULATION EXAMPLE

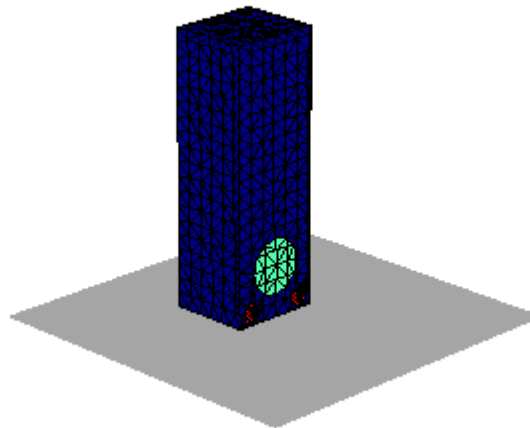
Normal particle velocity @80 Hz



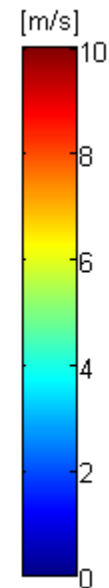
Free-Field



3U1 full-space

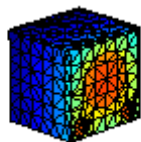


3U1 half-space

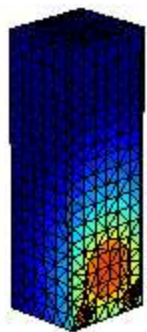


# BEM CALCULATION EXAMPLE

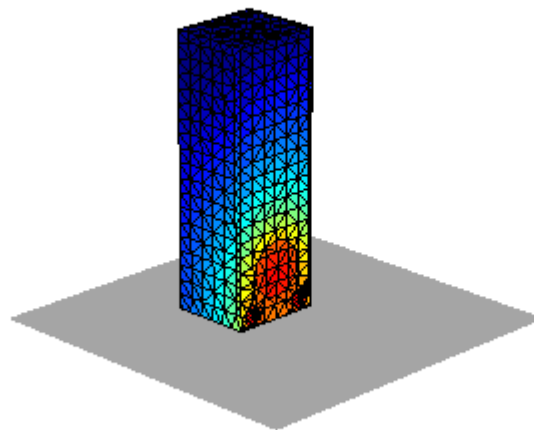
SPL @80 Hz



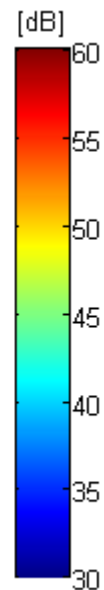
Free-Field



3U1 full-space

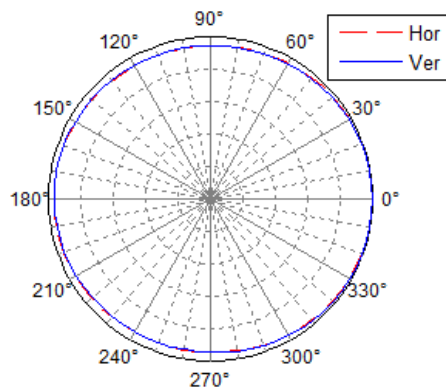


3U1 half-space

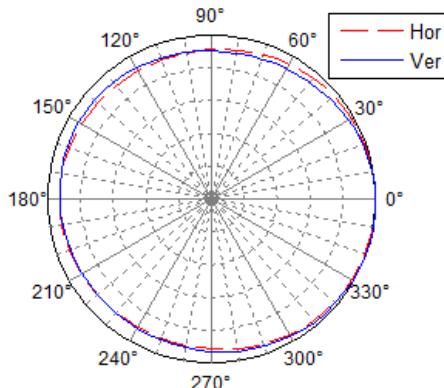


# BEM CALCULATION EXAMPLE

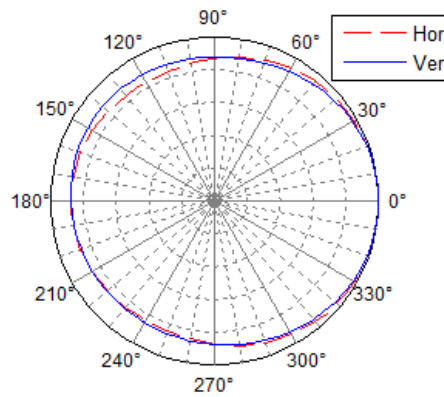
Balloon @80 Hz



Free-Field



3U1 full-space

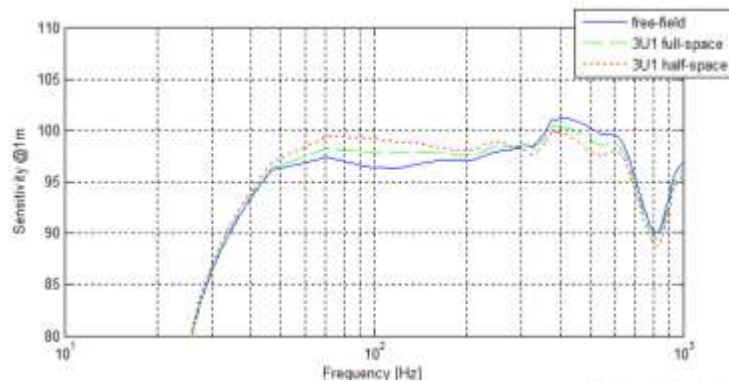


3U1 half-space

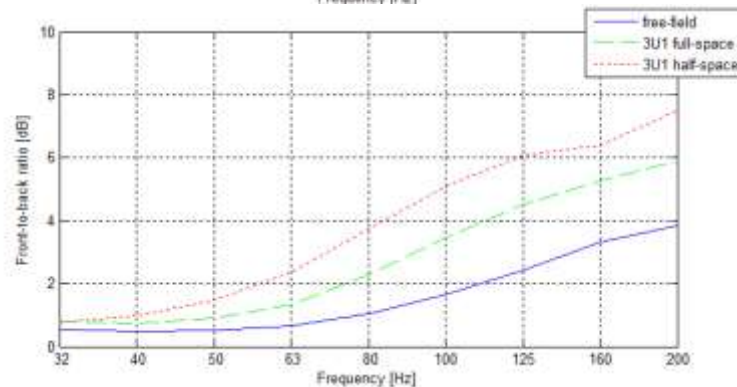


# BEM CALCULATION EXAMPLE

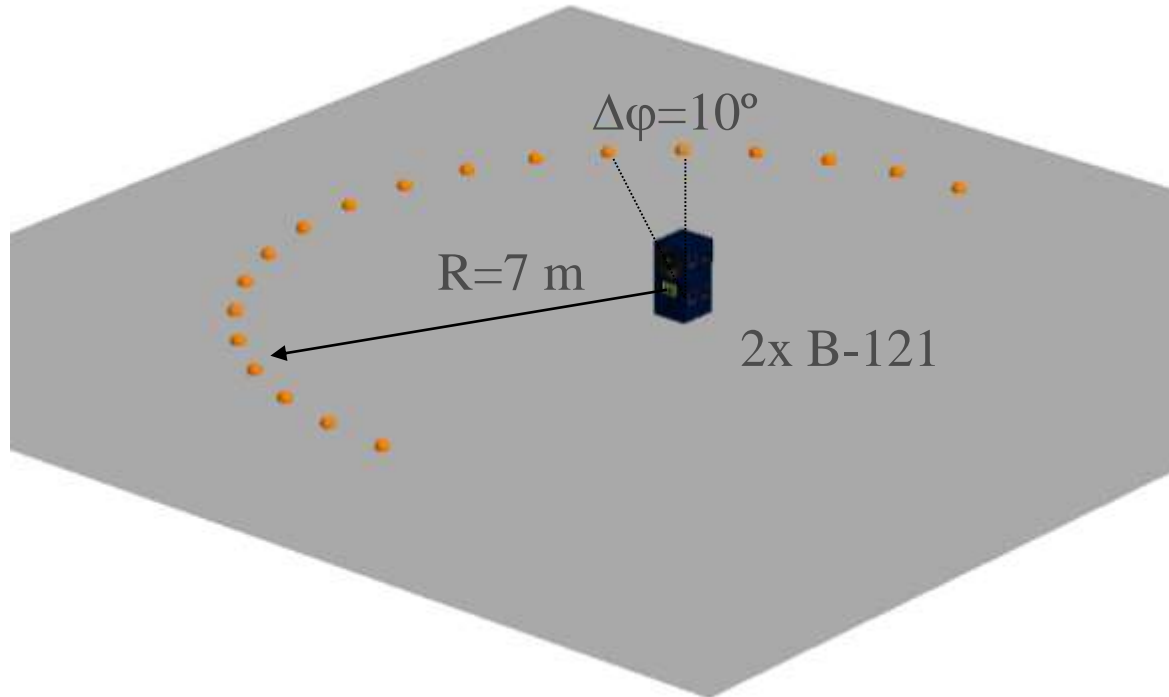
Sensitivity



Front-to-back ratio



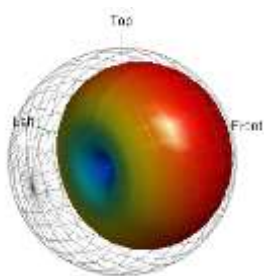
# VALIDATION PSM-BEM MODEL



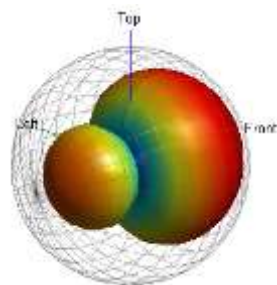
# VALIDATION PSM-BEM MODEL

Theoretical

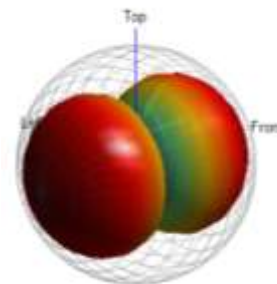
Cardioid



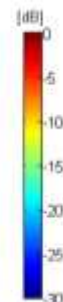
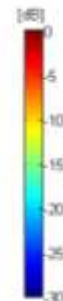
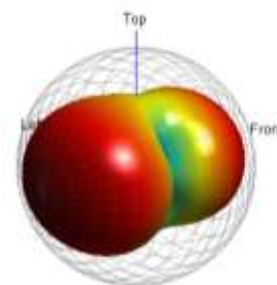
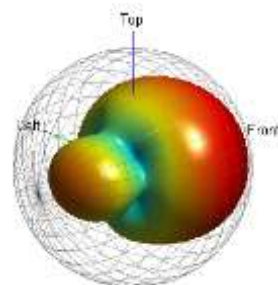
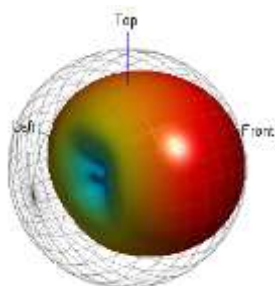
Hyper-cardioid



Dipole



Predicted  
(63 Hz octave)



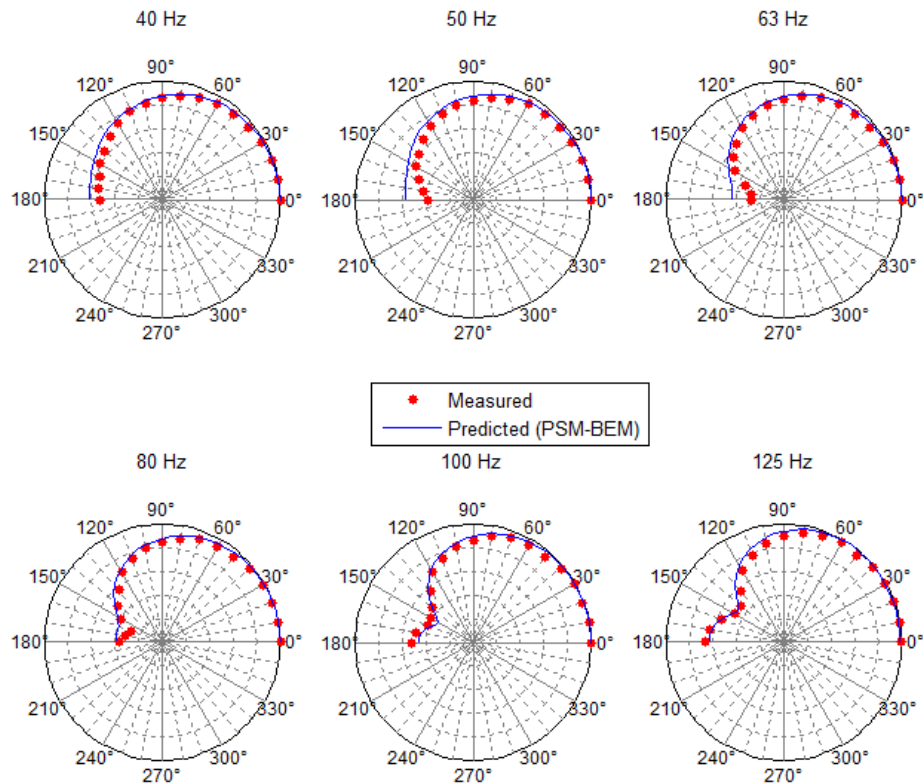
# MEASUREMENT RESULTS

## Cardiod setting

Mean array parameters:

DI = 4.9 dB

$G_{\text{array}} = 1.4 \text{ dB}$



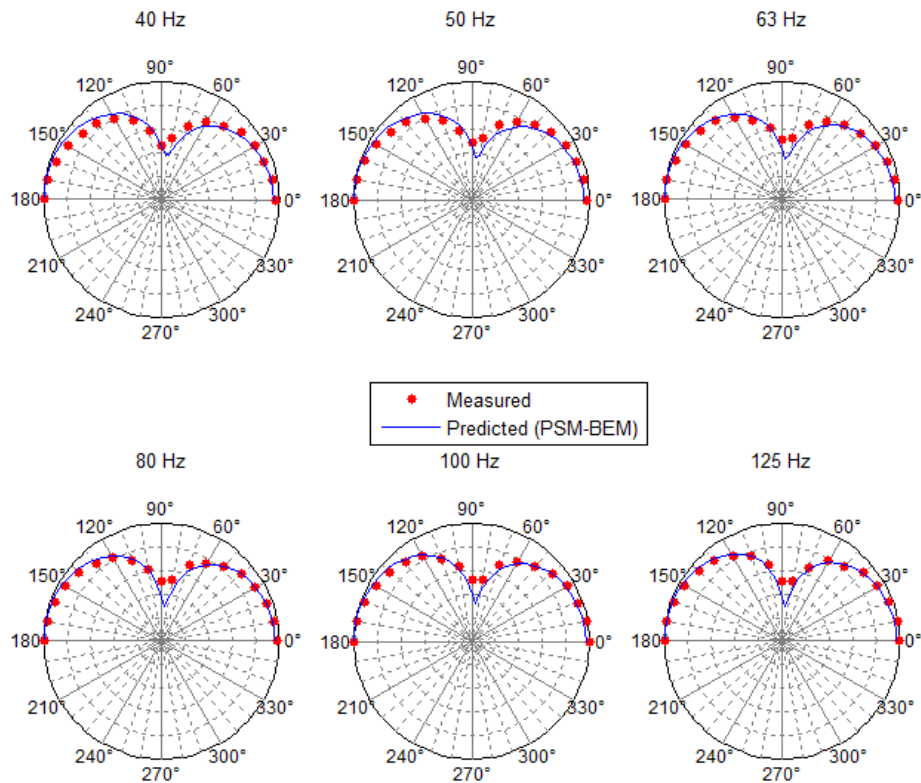
# MEASUREMENT RESULTS

## Dipole setting

Mean array parameters:

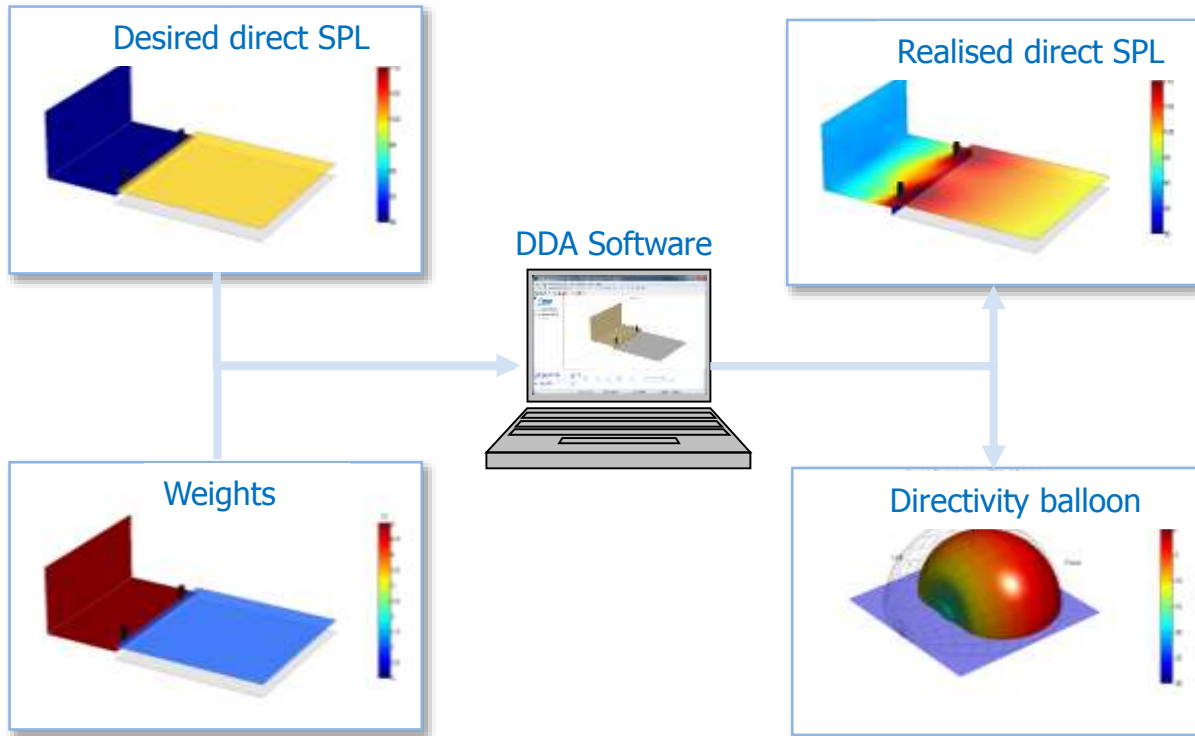
DI = 5.3 dB

$G_{\text{array}} = -0.5$  dB



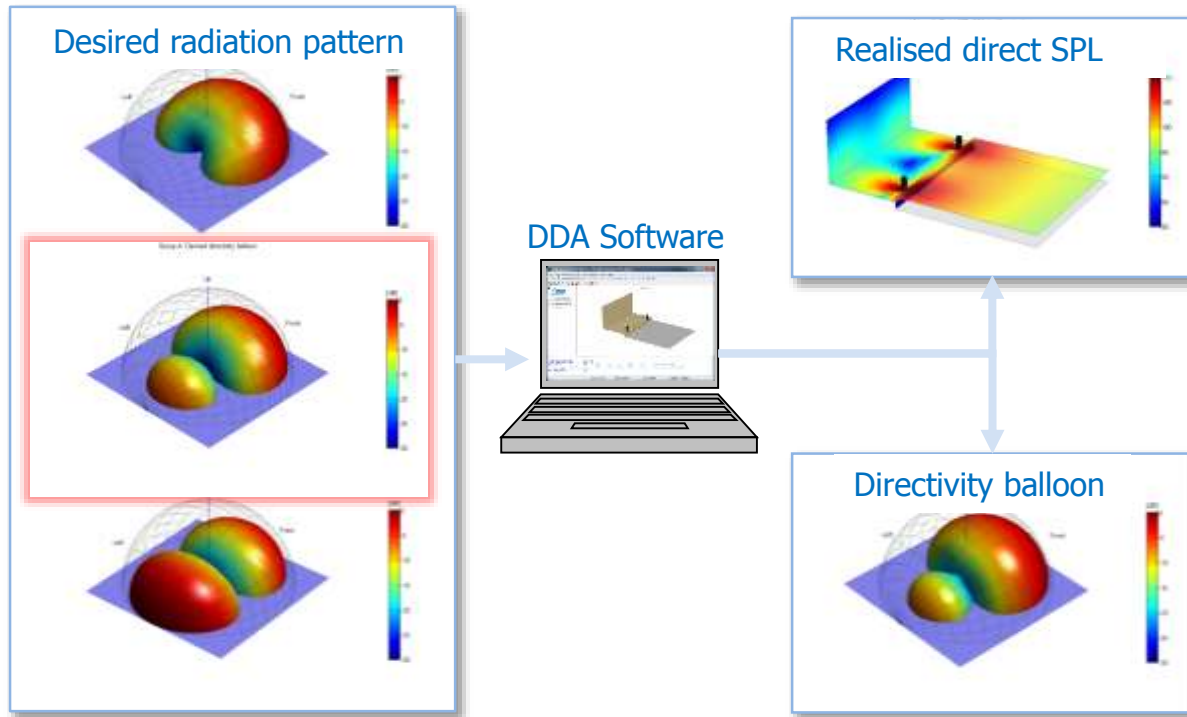
# HOW DOES IT WORK IN PRACTICE?

## DDS Geo method



# HOW DOES IT WORK IN PRACTICE?

## DDS Balloon method



# Summary & Conclusions

- Hybrid PSM-BEM model handles
  - Full-space
  - Half-space
  - Various array lengths
- Very accurate modelling of beam-shaped differential subwoofer arrays
- Large front-to-back ratio of cardioid subwoofer arrays
- Good Robustness, i.e. array response not sensitive to small deviations in sensitivity of individual drivers